A possible high-temperature origin of the ² Moon and its geochemical consequences

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Abstract. The formation of the Moon is thought to be the result of a giant impact between 11 a Mercury-to-proto-Earth-sized body and the proto-Earth. However, the initial thermal 12 state of the Moon following its accretion is not well constrained by geochemical data. 13 Here, we provide geochemical evidence that supports a high-temperature origin of the 14 Moon by performing high-temperature (1973-2873 K) metal-silicate partitioning 15 experiments, simulating core formation in the newly-formed Moon. Results indicate that 16 the observed lunar mantle depletions of Ni and Co record extreme temperatures (>2600-17 3700 K depending on assumptions about the composition of the lunar core) during lunar 18 core formation. This temperature range is within range of the modeled silicate evaporation 19 buffer in a synestia-type environment. Our results provide independent geochemical 20 support for a giant-impact origin of the Moon and show that lunar thermal models should 21 start with a fully molten Moon. Our results also provide quantitative constraints on the 22 effects of high-temperature lunar differentiation on the lunar mantle geochemistry of 23 volatile, and potentially siderophile elements Cu, Zn, Ga, Ge, Se, Sn, Cd, In, Te and Pb. 24 At the extreme temperatures recorded by Ni and Co, many of these elements behave 25

insufficiently siderophile to explain their depletions by core formation only, consistent with
 the inferred volatility-related loss of Cr, Cu, Zn, Ga and Sn during the Moon-forming event
 and/or subsequent magma-ocean degassing.

29 Keywords: Moon, Core formation, Giant Impact, Siderophile, Accretion, Volatiles

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1. INTRODUCTION

The giant impact model of Moon formation is predominantly studied with hydrodynamic 32 simulations (Cameron and Ward, 1976; Benz et al., 1986; Canup, 2012; Cuk et al., 2016; 33 Lock et al., 2018). Several groups have specifically studied the evolution of the Moon-34 forming material following the giant impact (Charnoz and Michaut, 2015; Lock et al., 2018; 35 Nakajima and Stevenson, 2018), and suggest that initial temperatures of this material are 36 extremely high. The thermochemical models in Nakajima and Stevenson (2018) suggest 37 that peak temperatures within the mid-plane disk could have been up to 4000-4500 K. 38 On the other hand, Rufu et al. (2017) suggested that the Moon could have been formed 39 by a succession of smaller impacts on the proto-Earth, which would likely result in lower 40 peak temperatures of Moon-forming materials. The most recent lunar formation models 41 suggest the Moon formed in a cloud of vaporized rock moving at a high angular 42 momentum formed directly after a high-energy impact between the proto-Earth and the 43 impactor (Lock et al., 2018). 44

Geochemical evidence for the conditions accompanying a giant impact is qualitative at present. The strongest geochemical evidence for the occurrence of a Moon-forming giant impact stems from measurements of very small but detectable differences in the isotopic composition of volatile elements between primitive lunar materials and terrestrial

samples (Paniello et al., 2012; Wang and Jacobsen, 2016; Kato and Moynier, 2017; 49 Pringle et al., 2017). Although their isotopic compositions in lunar samples provide 50 fundamental clues to the ambient thermal regime at some stage of lunar formation, these 51 geochemical data do not provide specific constraints on the thermal state of the Moon 52 directly after the Moon-forming event. For some of these elements their isotopic 53 54 compositions may have been altered in much later stages during lunar evolution (Paniello et al., 2012; Kato and Moynier, 2017; Sossi et al., 2018), e.g., during crystallization of the 55 lunar magma ocean (LMO). For example, chromium isotopic compositions of primitive 56 lunar rocks have been used to argue for low-temperature degassing of Cr following 57 formation of the Moon (Sossi et al., 2018), whereas models for other isotopic systems 58 (e.g., Wang and Jacobsen, 2016) have been used to support the hypothesis of a very hot 59 (i.e., > 3500 K) origin of the Moon (Lock et al., 2018). 60

61 Current estimates of early Moon temperatures range from cool enough to only enable 62 shallow, partial melting, to sufficiently high to lead to whole-Moon melting (e.g., Longhi, 63 2006; Steenstra et al., 2016; Charlier et al., 2018). Some experimental studies of LMO 64 crystallization have been used to argue for shallow melting (Charlier et al., 2018), but the 65 outcome of these models depends strongly on a variety of assumptions, including the 66 efficiency of crystal-melt separation, water content in the LMO and crystallization regime 67 (Lin et al., 2016; Charlier et al., 2018; Rapp and Draper 2018).

Here, we attempt to constrain temperatures in the early Moon by assessing the temperatures during core formation, which is the first major differentiation event in the Moon after its accretion. To this end we performed high-temperature (1973–2873 K) metal-silicate partitioning experiments at high pressure, simulating core formation in the newly-formed Moon, and assessing the core-mantle distribution of a range of non-volatile
and volatile siderophile trace elements (Ni, Co, Cu, Zn, Ga, Ge, Se, Sn, Cd, In, Te and
Pb).

Siderophile elements have been shown to be a valuable tool for studying the thermal 75 regime during the earliest differentiation of the Earth (e.g., Wade and Wood, 2005) and 76 other planetary bodies (e.g., Chabot and Agee, 2003). Previous siderophile element 77 studies related to the Moon generally assumed a significant impactor contribution to the 78 lunar siderophile element budget (O'Neill et al., 1991; Rai and van Westrenen, 2014; 79 Steenstra et al., 2016), but to date definitive geochemical evidence to support such a 80 contribution has not been found (e.g., Kruijer et al., 2015). On the other hand, multiple 81 elemental and isotopic lines of evidence indicate a bulk silicate Earth (BSE) - like bulk 82 Moon composition, at least in terms of non-volatile elements (e.g., Ti, Zhang et al., 2012; 83 W, Kruijer et al., 2015; O, Young et al., 2016). A strong geochemical link between the 84 BSE and the bulk Moon is also inferred from current ideas and dynamical models of lunar 85 formation (Canup, 2012; Cuk and Stewart, 2012; Lock et al., 2018), isotopic similarities 86 of refractory elements between BSE and bulk Moon (e.g., O, Ti, Fe, W; Zhang et al., 2012; 87 88 Kruijer et al., 2015; Young et al., 2016; Sossi and Moynier, 2017) and similarity in abundances of major and trace elements between the BSE and BM, including virtually 89 the whole class of refractory lithophile elements (Dauphas et al., 2014). 90

Here, we leverage this equality between bulk Moon and BSE composition for refractory elements to estimate the temperature during core formation in the Moon, using the elements Ni and Co. It is well established that these elements are depleted in the lunar mantle relative to BSE (Delano, 1986; Jones and Palme, 2000; Sossi et al., 2018).

However, their depletions are much smaller than expected given their siderophile 95 behavior at temperatures of up to ~2000 K (Kegler et al., 2008; Siebert et al., 2011), 96 especially given that the lunar core is likely to be sulfur-poor (Righter et al., 2017; 97 Steenstra et al., 2018; Brenan et al., 2019). Previous metal liquid-silicate melt partitioning 98 experiments have shown that the siderophile behavior of Co and Ni is affected by changes 99 100 in pressure and temperature (P-T), whereas it is largely unaffected by changes in silicate melt composition and oxygen fugacity (fO₂) given their 2+ valence states (Thibault and 101 Walter, 1995; Kegler et al., 2008; Siebert et al., 2011). Due to their non-volatile nature, Ni 102 and Co abundances in the Moon are unlikely to have been significantly affected by 103 volatility-related fractionation processes. In contrast to other non-volatile elements such 104 as the highly siderophile elements, the high abundances of Co and Ni in the lunar mantle 105 exclude significant disturbance of their concentrations through addition of a late veneer 106 significantly post-dating Moon formation. Their metal-silicate partitioning behavior is likely 107 unaffected by changes in silicate melt composition, in contrast to other refractory 108 elements such as Mo and W (Kegler et al., 2008; Siebert et al., 2011; Steenstra et al., 109 2017a). Given the 2+ valence state of Co and Ni under lunar-relevant fO₂, the relative 110 111 depletions and ratios of these elements are independent of the fO₂ during lunar differentiation (e.g., Siebert et al., 2011). The depletions of Ni and Co in the lunar mantle 112 113 therefore provide a unique opportunity to constrain the initial thermal state of the Moon 114 during core formation. Using our Ni and Co-based models, we also assessed to what extent the lunar mantle depletions of the other, more volatile and potentially siderophile 115 elements could reflect high-temperature lunar core formation. 116

117 **2. METHODS**

118 **2.1 Experimental approach**

To better constrain the effect of temperature on the metal liquid-silicate melt partition 119 coefficients of Co, Ni and a variety of other trace elements for lunar silicate melt 120 compositions, we performed high-pressure, high-temperature experiments in a 1500-ton 121 multi-anvil apparatus at the Geophysical Laboratory, Carnegie Institution for Science at 122 temperatures between 1973 and 2873 K and pressures of 3.2-3.9 GPa (Table 1). 123 Experiments were conducted using 18mm edge length Cr-doped MgO or ZrO₂ octahedra, 124 graphite heaters and polycrystalline 1.6 mm I.D. MgO capsules. Capsules were loaded 125 with a synthetic powdered analogue of primitive lunar Apollo 15 green glass (Delano, 126 1986) and Fe metal doped with a range of trace elements, mixed in a volume 2:1 ratio. 127 Two metal compositions were used (see Table 1). 128

Samples were pressurized to peak pressures before heating. Pressure calibration was 129 based on the gtz-coes and gt-pv transitions, resulting in an estimated pressure 130 uncertainty of ~0.2 GPa. Temperature was monitored using a Type C (95%W/5%Re -131 74%W/26%Re) thermocouple placed directly above the sample container at the assembly 132 hotspot. Metal-silicate mixtures were sintered at 1273 K for 60 to 120 min to reduce 133 134 porosity of the MgO capsule, and subsequently heated to target temperature. Above 2473 K, experimental temperatures were estimated using well-defined power-temperature 135 136 relationships (Appendix section A.1; Fig. S.1). Experiments were run at peak conditions 137 between 10 and 0.5 min, depending on final temperature. Although no time-series was performed, these run durations have previously been shown to be sufficient for attainment 138 of metal liquid-silicate melt equilibrium at these extreme temperatures (Thibault and 139 140 Walter, 1995; Wade and Wood, 2005; Siebert et al., 2011). Experiments were rapidly

quenched by shutting off the power to the furnace. Recovered samples were mounted in
 petropoxy resin, polished using different grades of AI polishing powder and analyzed
 using EPMA and laser ablation ICPMS (inductively coupled plasma mass spectrometry)
 techniques.

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146 **2.2 Analytical approach**

Major element abundances of metals and silicates were determined using JEOL JXA-147 8530F electron probe microanalyses at the University of Münster, Germany and at the 148 Dutch National Geological Facility at Utrecht University, and are summarized in Tables 149 S.1 and S.2. Metal alloys and silicate melts were analyzed with a defocused 15 µm 150 diameter beam. The analyses were done using beam currents of 20 nA and an 151 accelerating voltage of 15 kV. Counting times were 30 s for peak and 15 s for background 152 for major elements. Measurement points were set in lines and/or raster grids, depending 153 of the available surface area of the analysed phases, with step sizes approximately 154 equivalent to spot sizes. A set of synthetic and natural silicate and metal reference 155 materials were used for standardization. Data reduction was performed using the $\Phi(\rho Z)$ 156 157 correction. Additional details related to the EPMA analyses are provided in Appendix section A.2. 158

LA-ICP-MS analyses were performed at the University of Münster to quantify the abundances of trace elements in the metal liquids and silicate melts (Tables S.1, S.2). Analyses were performed using a 193 nm ArF excimer laser (Analyte G2, Photon Machines) with a repetition rate of 10 Hz and energy of \sim 3–4 J/cm² throughout the entire analytical session with beam diameters ranging between 25–50 µm. The following isotopes were measured: ²⁹Si, ³¹P, ⁴³Ca, ⁴⁹Ti, ⁵¹V, ⁵³Cr, ⁵⁵Mn, ⁵⁹Co, ⁶⁰Ni, ⁶¹Ni, ⁶³Cu, ⁶⁶Zn,
⁶⁹Ga, ⁷³Ge, ⁷⁵As, ⁸²Se, ⁹³Nb, ⁹⁵Mo, ¹¹⁸Sn, ¹²¹Sb, ¹²⁵Te, ¹⁸¹Ta, ¹⁸²W and ²⁰⁸Pb. The NIST
612 glass was used as an external reference material for both metal alloys and silicate
melts. Concentrations of Si in the silicate melt and Ni in the metallic liquid were used as
internal standards. The USGS reference materials BIR-1G and BCR-2G were analyzed
every ~20 LA-ICP-MS spots to assess the analytical accuracy and precision of measured
trace element concentrations (Fig. S.2).

The use of non-matrix-matched primary standards requires corrections on measured 171 concentrations of volatile and highly refractory elements in metals. Steenstra et al. (2019) 172 showed that the extent of elemental fractionation during LA-ICP-MS of iron-rich metal 173 analyses is most significant for the most volatile (e.g., Se, Te, Cd, Pb) and most refractory 174 elements (i.e., Mo, W). Neglecting these matrix effects would result in significant 175 overestimation of the $D_i^{met \, liq-sil \, melt}$ values. Abundances of volatile elements in metals 176 were therefore corrected downwards using the empirical correction factors reported in the 177 latter study (Steenstra et al., 2019). 178

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180 **3. RESULTS**

3.1 Run products and metal liquid-silicate melt partition coefficients

Run products show well-segregated metallic blobs in a quenched silicate melt (Fig. 1). All silicate melts quenched to a heterogeneous phase with spinifex olivine crystals and interstitial glass. Ferropericlase crystals (Mg,Fe)O were commonly formed due to the increase of the MgO content of the silicate melt through interaction of the silicate melt with the MgO capsule at high temperature conditions. The increase of the silicate melt MgO content due to capsule interaction also resulted in a substantial decrease of CaO and Al₂O₃ contents, compared to the initial starting composition (Fig. S.4). No evidence for metal zoning was observed, although smaller-scale (<5–10 um) heterogeneities were observed, as typically observed for quenched metal alloys.

Metal liquid-silicate melt partition coefficients of Co, Ni and the other trace elements were treated as exchange coefficients by considering the following equilibria (e.g., Wade and Wood, 2005):

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$$MO_{n/2}^{silicate} + \frac{n}{2}Fe^{metal} = \frac{n}{2}FeO^{silicate} + M^{metal}$$
 (1)

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where M or MO is the element or oxide considered with its corresponding valence *n*. Taking the logarithm of the equilibrium constant ($K_{app}^{met \, liq-sil \, melt}$) results in Eq. (2):

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$$200 \quad \log K_{\rm app}^{\rm met\,liq-sil\,melt} = \log \frac{(x_{\rm Fe0}^{\rm sil\,melt})^{n/2} \cdot (x_{\rm M}^{\rm met\,liq})}{(x_{\rm MO}^{\rm sil\,melt}) \cdot (x_{\rm Fe}^{\rm met\,liq})^{n/2}} + \log \frac{(\gamma_{\rm M}^{\rm met\,liq})}{(\gamma_{\rm Fe}^{\rm met\,liq})^{n/2}} + \log \frac{(\gamma_{\rm Fe0}^{\rm sil\,melt})^{n/2}}{(\gamma_{\rm MO}^{\rm sil\,melt})}$$
(2)

201

where x are molar fractions, n is the valence of the element considered and γ are the 202 activity coefficients of Fe and trace element *M*. Valences were assumed to be 1+ for Cu, 203 2+ for Ni, Co, Cr, Zn, Ge, Cd, Sn, Pb and 3+ for Ga and In (e.g., Siebert et al., 2011). 204 Note that the above approach directly accounts for variable fO_2 between the experiments. 205 Activity coefficients of Ni, Co and Cr in the metal ($\gamma_M^{met \, liq}$) at a given temperature for a 206 given metal composition were calculated using a thermodynamic approach that 207 interactions different 208 incorporates the between the elements

(http://norris.org.au/expet/metalact/; Wade and Wood, 2005). Interaction parameters ($\gamma_{M}^{met liq}$) describing the interaction of the various volatile elements (Cu, Zn, Ga, Ge, Se, Cd, In, Sn, Te, Pb) in the metal phase are not well or not constrained at all. We therefore assumed their activity to be unity in the metal phase, which is justified by the great similarity of $K_{app}^{met liq-sil melt}$ values for these elements for different metal compositions (see section 3.3 and related figures).

The doping levels of the elements considered in the Fe-rich alloys (Table S.2) are insufficient to result in a meaningful change of $\gamma_{\text{Fe}}^{\text{met liq}}$; all of the Fe activity coefficient values calculated for the experiments are equal to unity, demonstrating the absence of significant element interactions in the experimental alloys (Table 1). Similar results were found for Ni, Co and Cr.

The $\gamma_{MO}^{sil melt}$ values were taken from previous studies and/or calculated using 220 thermodynamic models. For modeling and parameterization of equilibrium constants and 221 metal liquid-silicate melt partition coefficients, values of $\gamma_{\rm FeO}^{\rm sil\,melt}$ = 1.7 and $\gamma_{\rm NiO}^{\rm sil\,melt}$ = 3.7 222 were assumed (Holzheid et al., 1997; Colson, 2017). These values are appropiate for the 223 lunar mantle during core formation and for the experimental silicate melt compositions 224 obtained in this study. To describe the activity of $\gamma_{CrO}^{sil\,melt}$, we used a thermodynamic model 225 that describes its dependency as a function of $\gamma_{Ni0}^{sil \,melt}$ (O'Neill and Berry, 2006). The 226 activity of CoO was modeled as a function of $\gamma_{NiO}^{sil melt}$ given the strong correlation of these 227 parameters ($\gamma_{CoO}^{sil melt}$ = 0.30 * $\gamma_{NiO}^{sil melt}$) (Holte et al., 2018). 228

Finally, the metal-silicate partitioning behavior of Se and Te is not directly dependent on *f*O₂ (Rose-Weston et al., 2009) and for these elements we considered metal-silicate partition coefficient D (defined as the ratio between the concentration (in wt.%) of element *i* in the metal, relative to the concentration (in wt.%) of element *i* in the silicate melt).

3.2 The effect of temperature on the siderophile behavior of Ni, Co and Cr in lunar systems

Fig. 2 shows $K_{app}^{\text{met liq-sil melt}}$ values for Ni, Co, Cr as a function of temperature. Our data 236 obtained at approximately constant pressure shows that increasing temperature greatly 237 increases the siderophile behavior of nominally lithophile element Cr and strongly 238 decreases the iron-loving tendencies of Ni and Co (Table 2). At 5 GPa, the pressure 239 corresponding to the present-day lunar core-mantle boundary (Weber et al., 2011), a best 240 fit to our new data in combination with lower temperature data for lunar melts yields the 241 fit parameters listed in Table 2 (obtained using Eq. 2). The calculated $K_{abb}^{met \, liq-sil \, melt}$ 242 values and temperature terms generally agree with those derived in previous studies for 243 non-lunar silicate melt compositions (e.g., Wade and Wood, 2005; Kegler et al., 2008; 244 Siebert et al., 2011). Wade and Wood (2005) reported temperature terms of 3100 and 245 2500, without uncertainties, for Ni and Co based on free-energy calculations. Siebert et 246 al. (2011) reported temperature terms of 2900±300 for Ni, 1900±250 for Co and 247 -3300±500 for Cr based on multiple linear regressions. Kegler et al. (2008) reported 248 temperature terms for Ni and Co for <5 GPa data of 4600±400 and 2000±300. Thus, in 249 case of Co and Cr, our results (2228±156; -3810±505, respectively) are generally within 250 error with those previously derived. The temperature term derived for Ni in this study 251 (5379±231) is higher than previous studies. This is most likely explained by the variability 252 253 in the effects of temperature on the metal-silicate partitioning behavior of Ni as a function

of pressure, as proposed by Kegler et al. (2008), and by the fact that Siebert et al. (2011) 254 incorporated Ni data obtained under a wide range of pressures (<25 GPa). Kegler et al. 255 (2008) found that the magnitude of temperature effects on $D_{Ni}^{\text{met liq-sil melt}}$ decreases with 256 pressure, which results in near-negligible effects of temperature at very high pressures 257 (>25 GPa), consistent with the much lower temperature term for Ni derived by Siebert et 258 al. (2011). Comparing our partitioning results for Ni, Co and Cr obtained for lunar 259 compositions with previous results obtained for terrestrial compositions at a given 260 temperature suggests that the effects of silicate melt composition on their activities in the 261 silicate melt are limited within the compositional range considered. For Ni, Co and Cr this 262 observation is consistent with previous metal-silicate partitioning coefficients obtained for 263 a large variety of melt compositions, confirming that silicate melt compositions have 264 (near)-negligible effects on $D_{Ni, Co, Cr}^{met liq-sil melt}$ (Siebert et al., 2011; Steenstra et al., 2017a). 265

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3.3 The effects of temperature on the distribution of volatile elements between metal liquid and silicate melt

Figure 3 shows the $D_i^{met\,liq-sil\,melt}$ values (Se, Te) and $K_{app}^{met\,liq-sil\,melt}$ as a function of 269 temperature. The results show that Se and Te behave significantly less siderophile at a 270 given pressure with increasing temperature, consistent with previous experimental 271 observations within a smaller temperature range (Fig. 3; Rose-Weston et al., 2009). The 272 273 results also show that the siderophile behavior of Cu, Sn and Ge are decreased with increasing temperature (Table 2). The temperature term obtained for Cu (2485±820) is 274 lower than the experimental results of Mahan et al. (2018) obtained for terrestrial 275 compositions within a wider pressure range (~4150±300). The temperature term derived 276

for Ge in this study (~8000±1450) is more significant than that derived by Siebert et al. 277 (2011) (~4500±390). The increase of the siderophile behavior of Zn, Cd and Pb with 278 temperature is consistent with previous experimental results for terrestrial compositions 279 from of Siebert et al. (2011), Ballhaus et al. (2013) and references therein. The metal-280 silicate partitioning behavior of In and Ga (not shown in Fig. 3) are unaffected by changes 281 in temperature within the studied range (Table 2), which is also consistent with previous 282 results derived for terrestrial compositions (e.g., Siebert et al., 2011; Ballhaus et al., 283 2013). Overall, it is observed that the derived temperature effects are consistent with the 284 Arrhenian behavior of elemental partitioning, with non-siderophile elements showing an 285 increase of their siderophile behavior with increasing temperature, and vice versa. 286

287

288 4. DISCUSSION

4.1 Constraints on thermal regime during primordial differentiation of the

290 **Moon**

First, we re-assess the thermal regime during lunar differentiation using our new experimental results. Molar metal liquid-silicate melt partition coefficients (D_M^*) for Cr, Co and Ni were modeled using Eq. 3 (e.g., Siebert et al., 2011), with the newly derived temperature dependencies:

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$$\log D_{\rm M}^* = a + b(1/T) - \frac{n}{2} \log \left(x_{\rm FeO}^{\rm sil\,melt} / x_{\rm Fe}^{\rm met\,liq} \right) - \log \left(\gamma_{\rm M}^{\rm met\,liq} / (\gamma_{\rm Fe}^{\rm met\,liq}) \right)$$
(3)

For $x_{\text{FeO}}^{\text{sil melt}}$ we assumed the values appropriate for the lunar silicate mantle ($x_{\text{FeO}}^{\text{sil melt}}$ = 0.08±0.02; Rai and van Westrenen, 2014, and references therein), whereas $x_{\text{Fe}}^{\text{met liq}}$ was assumed to be 0.85, consistent with a Ni abundance of $x_{\text{Ni}}^{\text{met liq}}$ of 0.15 (Steenstra et al.,

2017b). This mantle FeO - core Fe range corresponds with an overall fO_2 of lunar 300 differentiation of -2.08±0.22 units below the iron-wüstite buffer, consistent with values 301 derived in previous studies (e.g., Steele et al., 1992; Karner et al., 2006; Rai and van 302 Westrenen, 2014; Steenstra et al., 2016). The activities of Fe, Ni, Co and Cr in the metallic 303 liquids ($\gamma_{Fe, Ni, Co, Cr}^{met liq}$) as a function of core composition were again calculated using a 304 thermodynamic approach (Wade and Wood, 2005) for each modeled temperature and 305 assumed lunar core composition, yielding an internally consistent thermodynamic model. 306 D_{M}^{*} values from Eq. (3) were compared with lunar core-silicate Moon partition coefficients 307 (D_{c/m})'s that would be required to explain the observed depletions of Cr, Co and Ni in the 308 silicate Moon by core formation: 309

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$$D_{c/m(i)} = (C_{bulk Moon(i)} - xC_{bulk silicate Moon(i)})/(C_{bulk silicate Moon(i)}(1-x))$$
(4)

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where $C_{bulk Moon(i)}$ and $C_{bulk silicate(i)}$ are the concentrations of element *i* in the bulk Moon and bulk silicate Moon and *x* is the assumed mass fraction of the lunar mantle. The concentration of Co in the lunar mantle may be slightly lower or within error with that of BSE, reflected by the required D value of <1.52. All required D values were calculated assuming a BSE bulk Moon composition.

Fig. 4a-c shows the modeling results. For a Fe-Ni lunar core without any light elements with a mass of 1.5 to 2 wt.% of the Moon (Righter et al., 2017; Williams et al., 2014), the observed Ni, Co and Cr lunar mantle depletions can be explained by their preferential partitioning into the lunar core, but only at extreme temperatures (~3200±550 K). At the low pressure and reducing conditions inferred for lunar core formation, C and S would be the only light elements to partition into the lunar core in significant quantities. Lunar

seismic constraints have been used to argue for the presence of <6 wt.% of light elements 323 in the lunar core (Weber et al., 2011). Geochemical evidence suggests the lunar core S 324 content is likely <0.5 wt.% (Righter et al., 2017; Steenstra et al., 2017b). The addition of 325 2 wt.% S yields a similar range of core formation temperatures as those inferred for a 326 pure Fe-Ni lunar core (~3150±550 K; Fig.4d-f). Assuming 5 wt.% of S in the lunar core 327 also provides a satisfactory fit in terms of Ni, Co and Cr at a comparable extreme lunar 328 core-mantle differentiation temperature of ~3100±600 K. The Ni/Co ratios of the lunar 329 mantle can be reproduced through formation of a lunar core without S or C at slightly 330 lower temperatures (<2900 K) than those based on the models of absolute Ni, Co and Cr 331 abundances, whereas a lunar core with 2 or 5 wt.% S reproduces the present-day Ni/Co 332 ratio of the lunar mantle within the range of formation temperatures derived from absolute 333 abundances of Ni, Co and Cr (Fig. 5). Although it is unlikely from current geochemical 334 and geophysical constraints (Day, 2018; Ding et al., 2018; Righter et al., 2017; Steenstra 335 et al., 2017b; Steenstra et al., 2018), models with more than 5 wt.% S in the lunar core 336 could yield lower core formation temperatures. High amounts of S in the lunar core are 337 unlikely because of both the low S abundance in the lunar interior, as discussed in section 338 339 4.1 (Righter et al., 2017; Day, 2018; Ding et al., 2018; Steenstra et al., 2018) as well as the lack of significant loss (>10%) of S during the Moon-forming event as inferred from S 340 341 isotopic systematics of lunar basalts (Wing and Farguhar, 2015).

Geochemical evidence suggests that C concentrations in the lunar core are <4.6 wt.% and could be as low as 0.4 wt.% C (Righter et al., 2017; Steenstra et al., 2017b). The addition of 5 wt.% C to the lunar core would lower the temperature at which the Ni, Co and Cr lunar mantle depletions can be simultaneously satisfied to 2600±600 K. However, the actual concentration of C in the lunar core is likely to be much lower than 5 wt.% given
the potential loss of C during the Moon-forming event and the outcome of the geochemical
and geophysical studies performed by Righter et al. (2017).

Finally, it should be noted that Cr is not the limiting element in any of the models described here. Any loss of Cr during the Moon-forming event or subsequent lunar differentiation (Sossi et al., 2018) would therefore not affect the geochemical models described above.

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4.2 Uncertainties related to estimating the thermal state of lunar

355 differentiation by Ni/Co

Segregation of metal- and/or sulfide liquids from the lunar mantle at any stage after lunar 356 core formation could have affected the abundance and ratios of Ni and Co. However, 357 significant quantities of residual sulfides in low-Ti basalts and glasses source regions are 358 excluded by both low S abundances and elemental correlations of Ni, Co and Cu (Day, 359 2018; Ding et al., 2018; Steenstra et al., 2018), as it has been shown that these elements 360 behave only mildly compatible (Ni, Co) to mildly incompatible (Cu) in primitive lunar low-361 362 Ti magmatic samples. Although Wänke et al. (2018) and Brenan et al. (2019) showed that some of the low-Ti melts could have experienced saturation of a S-poor sulfide during 363 some stages of their magmatic evolution, Brenan et al. (2019) concluded that the modal 364 abundances of these phases were sufficiently low (approx. 10 ppm) to have no 365 measurable effect on the abundances of moderately siderophile elements such as Ni and 366 Co (Brenan et al., 2019). On the other hand, Xia et al. (2019) recently argued for 367 368 significant sulfide fractionation during lunar differentiation, based on the Cu isotope

composition of the silicate Moon. However, their model relies solely on the assumption of 3500–7500 ppm S in the bulk Moon (i.e., enrichment of bulk Moon to BSE by a factor of 13–27 in terms of S), which is inconsistent with current of lunar formation, bulk Moon compositions and geophysical properties of the lunar core (e.g., Steenstra et al., 2017b and references therein). We therefore conclude that the derived temperature range for the initial Moon is unlikely to be affected by potential metal- or sulfide saturation in the low-Ti basalt source regions.

It should also be assessed whether a shallow LMO and/or partial lunar core-silicate 376 melt equilibration could instead yield the Ni and Co abundances in the lunar interior. Due 377 to the negative effects of pressure on Ni and Co partitioning (Kegler et al., 2008; Siebert 378 et al., 2011), lower pressure shallow- or intermediate depth LMO scenarios (e.g., Charlier 379 et al., 2018) would increase the discrepancies between modeled and observed depletions 380 even further. Partial equilibration of the lunar core with the lunar mantle could result in 381 less strong mantle depletions of Ni and Co during core-mantle differentiation, but this 382 would be at odds with the measured lunar mantle HSE depletions and the proposed 383 replenishment of these elements during a late veneer on the Moon (Day et al., 2007; 384 385 Kruijer et al., 2015). Significant disequilibrium between lunar core and mantle would likely be reflected by proto-BSE (i.e., non-chondritic) signatures of HSE in lunar materials, 386 especially at the extent that is required to significantly disturb Co and Ni abundances in 387 388 the lunar mantle. A large degree of bulk silicate Moon homogenization is also consistent with the identical Sm-Nd isotopic equilibria observed in lunar samples derived from 389 distinctly different regions of the lunar interior (Borg et al., 2019). 390

The sensitivity of the outcome of our models to the effect of a late veneer should also 391 be assessed. The abundances of Ni and Co in the BSE and lunar mantle could have been 392 affected by the addition of chondritic late veneers of a 0.3 to 0.7 mass % (Bottke et al., 393 2010; Wang and Becker, 2015) to the Earth and 0.02 to 0.05 mass % (Kruijer et al., 2015) 394 to the Moon. In case of the bulk silicate Earth, such a late veneer would increase pre-late 395 veneer BSE Ni contents by 30 to 125 ppm and Co abundances by 1.5–6 ppm, the exact 396 amount depending on the composition of chondritic late veneer impactors (Newsom, 397 1995). Stripping out these amounts of Ni and Co from the (present-day) BSE values used 398 to model the composition of the bulk Moon, the metal-silicate partition coefficients 399 required to explain their depletions in the lunar mantle are even lower, implying higher 400 lunar core formation temperatures. For the Moon, a late veneer contribution corresponds 401 to the addition of approximately 2 to 9 ppm Ni and less than 0.5 ppm Co. The maximum 402 proposed extents of late veneers based on HSE abundances and W isotopes therefore 403 do not significantly alter the abundances of Ni and Co in the BSM. The high-temperature 404 differentiation of the Moon suggested by our calculations is therefore not affected by 405 assumptions about late veneer additions to Earth and Moon. 406

Finally, uncertainties in the actual fO_2 during lunar core formation could affect the modeled temperature range. In the above calculations a fO_2 of $\Delta IW = -2.08\pm0.22$ is assumed, based on the assumption that the FeO content of the bulk Moon is identical to that of the present-day bulk silicate Earth, as implied from Fe isotopes (Sossi and Moynier, 2017) as well as the overall geochemical similarity of the bulk silicate Earth and the bulk Moon (e.g., Zhang et al., 2012; Kruijer et al., 2015; Young et al., 2016). It should be noted that current density models of the lunar interior do permit a slight enrichment of

the bulk Moon compared to the present-day BSE (Dauphas et a., 2014), although the 414 corresponding uncertainties are significant. In this case, the modeled fO₂ would be closer 415 to $\Delta IW = -1.5$ or at maximum -1, thereby decreasing the modeled temperature range due 416 to less siderophile behavior of Ni and Co at such conditions. However, we again 417 emphasize that current geochemical evidence is not consistent with an FeO enrichment 418 419 of the bulk Moon compared to BSE.

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4.3 Lunar core formation at high temperatures

High-temperature lunar core formation (at temperatures of >2600 to up to 3700 K, 422 depending on the assumed light element content of the core) is thus the most plausible 423 process to explain the observed lunar mantle depletions of Ni and Co. This temperature 424 estimate is a lower limit as it reflects the last recorded stage of metal-silicate equilibrium 425 during lunar differentiation. In this scenario, it is assumed that the super-liquidus Ni and 426 Co signature of the lunar mantle was preserved due to rapid cooling of the lunar mantle 427 and core, relative to the timescales of convective mixing within the lunar interior, following 428 core formation. It should be noted that rapid crystallization of the lunar magma ocean is 429 430 also reflected by Sm-Nd systematics of primitive lunar samples (Borg et al., 2019). The only feasible mechanism to obtain such high temperatures during initial lunar 431 differentiation is through a high-energy giant impact. The proposed temperatures are 432 433 compatible with the evolution of BSE compositional vapors at pressures exceeding >20 bar, where the majority of lunar mass (> 80 per cent) has re-accreted to form the Moon 434 (Lock et al., 2018). High-temperature differentiation of the Moon is also consistent with 435 436 the existence of a deep, global lunar magma ocean inferred for the early Moon from

pristine volcanic glasses (Longhi, 2006) and with the extensive volatile loss during the
early evolution of the Moon, relative to other terrestrial bodies (Wang and Jacobsen,
2016; Kato and Moynier, 2017) (see also next section). Finally, it also reproduces the
required Hf/W of the silicate Moon (Thiemens et al., 2019) (see Appendix section A.5).

441

442 4.4 Siderophile behavior of volatile elements during a high-temperature Moon443 forming event?

In light of lunar core formation temperatures based on Ni and Co data, we assess to what 444 extent volatile elements Cu, Zn, Ga, Ge, Se, Cd, In, Sn, Te, Pb could have partitioned 445 into the lunar core during high temperature differentiation of the Moon. Modeling results 446 for a Fe-Ni lunar core (Fig. 6) show that at temperatures lower than ~2500–2700 K, the 447 lunar mantle depletions of Se, Cu, Te, Ge and Sn can be largely if not fully reconciled 448 with core formation only, generally consistent with our previous results (Steenstra et al., 449 2016, 2017c) (summarized in Fig. 7). This is extended to ~3200 K for Sn (Fig. 6). At higher 450 temperatures, increasingly more volatility-related loss of these elements is required for 451 explain their present-day abundances in the lunar mantle (Fig. 7). Due to the positive 452 453 effect of temperature on the siderophile behavior of Zn, Cd and Pb, required volatilityrelated loss slightly decreases with increasing core formation temperatures. However, it 454 is clear that no lunar core formation scenario can fully explain the depletions of the latter 455 elements and that significant volatility-related loss is required. These results are 456 consistent with the work of Righter (2019) and with the Zn isotopic composition of the 457 silicate Moon (e.g., Paniello et al., 2012; Day et al., 2019). 458

Figure 7 also shows that high-temperature core formation in the Moon may be a viable 459 mechanism to explain the apparent "overabundance" of some of these elements (Cu, 460 Ge, Se, Te, Sn) in the silicate Moon, compared to other elements of similar volatility (Wolf 461 and Anders, 1980; Hauri et al., 2015). It has been shown that at intermediate 462 temperatures of metal-silicate equilibration (~2200 K, Steenstra et al., 2016; 2017c), 463 464 virtually no volatility-related loss of the latter elements is required, as also indicated in Fig. 7. Indeed, volatility-related loss of both Cu and Sn during the formation and/or 465 differentiation of the Moon is strongly indicated from the light Sn and heavy Cu isotopic 466 compositions of lunar materials (Herzog et al., 2009; Wang et al., 2019). Lunar core 467 formation at super-liquidus temperatures may therefore be more consistent with observed 468 silicate Moon depletions of Cu, Se, Sn and Te, especially in light of recent results for other 469 similarly volatile elements (e.g., Day et al., 2019). 470

On the other hand, it has also been suggested that the abundances of the more 471 volatile siderophile- and chalcophile elements Ag, Bi, Cd, In, Sb, Sn, TI and Zn and their 472 CI chondritic-like proportions reflect a thin veneer of ordinary or CI-chondrite-like material 473 to the Moon (Wolf and Anders, 1980, O'Neill, 1991). However, in light of current 474 475 geochemical constraints on delivered late veneer mass (e.g., 0.02 to 0.05 mass %; Kruijer et al., 2015), it is deemed unlikely that the abundances of the majority of the elements of 476 interest in the lunar mantle would be significantly affected by a late veneer (Table S.3), 477 478 especially given their volatile nature and expected degassing upon impact.

479

480 **5. CONCLUSIONS**

The dependence of the metal liquid-silicate melt partitioning of Ni, Co, Cr and various 481 volatile trace elements (Cu, Zn, Ga, Ge, Se, Cd, In, Sn, Te, Pb) on temperature was 482 experimentally constrained at lunar-relevant pressures. The depletions of Ni and Co in 483 the lunar mantle, in conjunction their metal-silicate partitioning behavior at high 484 temperatures, indicate that studies of the thermal history of the Moon should start with a 485 superheated fully molten body. They also suggest that the geochemical composition of 486 the lunar mantle provides quantitative boundary conditions for the thermal state of the 487 Moon that can validate numerical models of Moon formation. Our experimental results 488 show that lunar core formation at high (>2650 K) temperatures, as inferred from Ni and 489 Co systematics, would require significantly (more) volatility-related loss of Cu, Ge, Sn and 490 most notably Se and Te, as their siderophile behavior would be significantly decreased, 491 compared to moderate lunar core formation temperatures (~2200 K). Core formation at 492 super-liquidus temperatures would result in slightly less required volatility-related loss of 493 Pb, Cd, whereas the abundances of Zn, In and Ga in the silicate Moon are virtually 494 unaffected by core formation, even at high temperatures. 495

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499 Acknowledgements

We would like to thank M. Duncan for her assistance in the experiments presented in this study. This work was supported by a Netherlands Organization for Scientific Research (N.W.O.) Vici award to W.v.W., a Carnegie Postdoctoral Fellowship to E.S.S. Experiments were also supported by NASA grant to Y.F. (NNX17AE30G) and by the DFG

- 504 (German Research Foundation) Project-D 263649064 SFB TRR-170 publication no.
- 505 93. We thank John Brodholt for editorial handling and thorough reviews by P. Sossi and
- an anonymous reviewer that significantly improved the quality of the manuscript.
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significant source of lunar material. Nat. Geosci. 5, 251–255.

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667 Figure captions

Fig. 1. Backscattered electron images of run products PR1518, PR1521 and PR1539.

669 Analytical spots from LA-ICP-MS analyses are visible in both metal and silicate phases.

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Fig. 2. The K^{met liq-sil melt} values of Ni, Co and Cr as a function of temperature from this study and previous studies. Exchange coefficients were normalized to 5 GPa using the pressure terms from a previous study (Siebert et al., 2011). High-temperature data (circles) from this study. Lower temperature data using similar capsules, lunar compositions and analytical tools were taken from Steenstra et al. (2017a, c). Errors are maximum errors calculated using simple error propagation while assuming 2 SE on EPMA and LA-ICP-MS concentrations.

678

Fig. 3. The $K_{app}^{met \, liq-sil \, melt}$ and $D_i^{met \, liq-sil \, melt}$ values of various volatile elements for lunar compositions as a function of temperature from this study and a previous study (Steenstra et al., 2017c). Errors are maximum errors calculated using simple error propagation while assuming 2 SE on EPMA and LA-ICP-MS concentrations.

683

Fig. 4. Modeled D_{Ni, Co, Cr}^{met liq-sil melt} values at 5 GPa as a function of temperature for (a-c) a
1.5 to 2 mass% Fe-Ni lunar core and (d-f) 1.5 to 2 mass%, 2 wt.% S bearing Fe-Ni lunar
core. Horizontal bars represent the values required to explain their depletions in the lunar

mantle by core formation (Table 2). Modeled D range includes uncertainties in fitting
 terms (see Table 2).

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Fig. 5. Modeled Ni/Co ratios as a result of lunar core formation versus temperature for a
1.5–2 mass% Fe-Ni lunar core with 2 wt.% S.

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Fig. 6. Modeled D_i^{met liq-sil melt} values for various volatile elements (obtained at ~3.8 GPa, normalized in case of Se and Te to 5 GPa) as a function of temperature for a 1.5 to 2 mass% Fe.Ni lunar core. Horizontal bars represent the values required to explain their depletions in the lunar mantle by core formation; modeled D range includes uncertainties in fitting terms (see Table 2).

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Fig 7. Modeled and measured elemental abundances of volatile (siderophile /chalcophile) 699 elements in the lunar mantle (in ppm) expressed as absolute concentrations (upper panel) 700 or normalized to bulk silicate Earth (lower panel). Elemental abundances were modeled 701 assuming (1) no core formation depletion (as indicated by triangles and grey solid line), 702 (2) by consideration of lunar core formation at -2.10±0.2 units below the iron-wüstite 703 buffer and 2200 K, corresponding to the approximate liquidus temperature at the lunar 704 core/mantle boundary (Rai and van Westrenen, 2014) (as indicated by blue squares and 705 the dine dashed line) and (3) by considering lunar differentiation at super-liquidus 706 temperatures (3500 K), as indicated by red squares and by the coarse dashed line. 707 Measured elemental abundances (green circles and corresponding fine-dashed line) 708 were taken from Hauri et al. (2015) and references therein (see Table 2). Previous bulk 709

- silicate Moon estimates from O'Neill (1991) and Ni et al. (2019), as indicated by light
- green diamonds and triangles, are plotted for comparison purposes.

Table 1 Experimental run conditions and measured metal-silicate partition coefficients. Numbers in brackets are errors in
 terms of least digits cited and calculated through simple error propagation while assuming 2 SE on EPMA and LA-ICP-MS
 analyses.

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Run #	Р	т	time	Comp. ^a	ΔIW ^b	D٥													
	(GPa)	(K)	(s)	•		Ni	Co	Cr	Cu	Zn	Ga	Ge	Se	Cd	In	Sn	Sb	Те	Pb
PR1446	3.3	2173	300	GG; A	-1.94	1193(65)	-	-	_	-	_	-	_	_	_	_	_	-	_
PR1449	3.9	2123°	300	GG; A	-2.49	2105(118)	-	1.08(14)	29(4)	1.37(8)	1.41(24)	-	27(5)	2.2(5)	8.3(15)	43(9)	5976(1612)	108(20)	8.6(22)
PR1450	3.8	2373	240	GG; A	-2.44	734(143)	-	1.09(19)	14.6(40)	1.64(16)	1.47(24)	-	13.4(55)	4.1(11)	8.4(38)	28(9)	1349(640)	15.2(58)	11.6(38)
PR1465	3.8	2460 ^c	180	GG; A	-2.47	1437(464)	-	1.06(42)	25(4)	1.17(8)	1.26(57)	-	11.1(50)	2.0(7)	12.1(43)	>12.2(8)	4241(3860)	14.3(67)	8.7(25)
PR1468	3.8	2073	120	GG; A	-1.82	1322(52)	-	-	5.5(16)	1.24(63)	_	-	28(7)	0.46(20)	8.5(11)	72(42)	25655(3116)	52(11)	1.42(51)
PR1470	3.8	2473	60	GG; B	-2.01	400(34)	174(9)	0.51(3)	14.6(19)	1.86(25)	2.66(56)	686(56)	_	-	_	35(13)	_	_	20(5)
PR1477	3.8	2273	120	GG; A	-2.19	795(59)	-	0.21(6)	32(10)	1.74(20)	2.83(83)	_	36(10)	3.0(8)	15.9(41)	22(6)	954(223)	79(20)	11.6(30)
PR1480	3.8	2473	60	GG; A	-2.19	558(132)	-	0.32(13)	25(9)	2.99(41)	6.2(18)	_	7.3(23)	5.5(23)	15.8(53)	>49(21)	910(313)	1.91(68)	25(14)
PR1481	3.8	2373	90	GG; B	-2.27	670(154)	283(35)	0.49(5)	-	-	-	750(354)	-	-	-	_	_	-	-
PR1489	3.8	2573°	75	GG; A	-2.42	678(115)	-	1.23(31)	18.4(47)	3.93(58)	3.11(85)	-	5.0(35)	7.1(25)	b.d.l.	>40(13)	4018(1415)	19(6)	24(10)
PR1491	3.8	2673 ^c	90	GG; A	-2.49	521(93)	-	0.50(10)	13.9(30)	1.66(15)	3.30(76)	-	1.80(82)	1.38(43)	13.8(44)	14(4)	6883(2380)	2.50(85)	9.7(34)
PR1505	3.8	2673 ^c	40	GG; B	-2.08	6450(695)	185(10)	0.57(4)	17.6(52)	1.13(20)	2.18(45)	566(72)	-	-	-	10.6(14)	-	-	13.8(23)
PR1506	3.8	2573°	60	GG; B	-2.09	4900(523)	156(6)	0.38(7)	12.1(19)	1.14(24)	2.54(59)	318(33)	-	-	-	8.5(12)	-	-	10.7(34)
PR1508	3.8	2773°	40	GG; A	-2.43	421(82)	-	1.64(16)	21(8)	3.83(35)	3.20(70)	-	4.8(13)	5.1(23)	19.1(54)	>42(11)	929(368)	5.0(19)	17.4(108)
PR1510	3.8	2773°	40	GG; B	-2.12	176(10)	113(6)	1.57(10)	9.9(22)	0.94(36)	b.d.l.	127(11)	-	-	-	10.9(31)	-	-	b.d.l.
PR1517	3.8	2773°	30	GG; B	-1.91	177(23)	111(14)	1.78(34)	15.1(28)	2.33(51)	4.57(94)	294(47)	-	-	-	-	-	-	15.8(47)
PR1518	3.8	2873°	30	GG; B	-2.05	201(13)	111(5)	0.70(6)	11.9(12)	1.36(19)	4.72(70)	386(27)	-	-	-	-	-	-	15.3(38)
PR1521	3.8	2873°	30	GG; B	-2.09	134(11)	84(7)	1.42(18)	10.2(22)	2.89(64)	5.15(32)	293(24)	-	-	-	-	-	-	23(5)
PR1522	3.2	2473	120	GG; A	-2.29	1141(133)	-	0.54(14)	21(5)	2.65(27)	3.49(34)	-	8.8(23)	3.8(15)	36(7)	47(7)	14309(5850)	19.0(43)	22(14)
PR1524	3.8	2773°	30	GG; A	-2.04	243(80)	-	0.64(14)	9.6(23)	3.42(27)	3.64(92)	_	2.51(106)	2.1(10)	15.7(66)	b.d.l.	1005(375)	2.94(123)	8.5(4.5)
PR1538	3.8	1973	600	GG; B	-1.51	1158(113)	241(13)	0.18(2)	6.3(12)	0.35(5)	1.52(26)	3175(368)	-	-	-	6.0(22)	_	-	2.7(7)
PR1539	3.2	2473	90	GG; B	-2.02	424(29)	181(11)	0.61(6)	22(7)	2.40(35)	b.d.l.	716(48)	-	-	-	-	-	-	28(5)
PR1561	3.8	2173	660	GG; A	-1.63	1800(62)	-	0.24(2)	46(6)	0.49(3)	1.55(24)	_	83(13)	0.88(15)	15.6(23)	34(9)	38921(9683)	311(63)	5.4(11)

^a GG = lunar Apollo 15 green glass; A and B denote the type of metal composition used in the experiments (A = Fe + 1 wt.% Si, 5 wt.% Ni, 1.5 wt.% As, Se, Cd, In, Sb, Te, Pb; B = Fe +

1.5 wt.% P, V, Cr, Mn, Co, Ni, Ge, Mo, W) ^b Calculated assuming $\gamma_{\text{Fe0}}^{\text{sil melt}} = 1.7 \,^{\circ}$ Temperature was estimated using power-*T* relationships derived with thermocouple at the same pressures and assembly; uncertainties are estimated to be ±50 K. ^o Measured metal-silicate partition coefficient D, defined here as the defined as the wt% ratio of element i in the metal liquid and

silicate melt, respectively.

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Table 2 Fitting results and abundances of the elements considered in the bulk silicate Earth (BSE) and in the bulk silicate 725 Moon (BSM) and corresponding log D values (calculated using Eq. 4) required to explain their lunar mantle depletions for 726 a 1.5 to 2 mass% lunar core. The log Kapp values (Ni, Co) and log D values (Se, Te) were prior to regressions normalized 727 to a common pressure of 5 GPa, respectively, using the pressure and/or FeO dependencies from Siebert et al. (2011) and 728 Steenstra et al. (2017c), respectively. 729

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	Α	B(1/T)	N	R ² ^a	bulk Moon abundance	bulk silicate Moon ^b	required log D core/mantle ^c
Cr ²⁺	0.51(24)	-3810(505)	31	0.61	2580±190 (ppm) ¹	2050±150 (ppm) ²⁻⁴	0.87±0.62
Co ²⁺	0.10(8)	2228(156)	17	0.91	103±4 ¹	90±18 ^{b3,4}	<1.52
Ni ²⁺	-1.16(11)	5379(231)	31	0.93	1900±80 ¹	505±85 ^{3,4}	2.21±0.18
Cu ¹⁺	0.17(32)	2564(819)	18	0.38	28±4 ¹	7.2±1.4 ³	2.26±0.04
Zn ²⁺	0.37(40)	-2873(988)	21	0.30	54±3 ¹	7.7±1.5 ³	2.59±0.33
Ga ^{3+ d}	_	_	-	-	4.3±0.2 ¹	2.3 ± 0.5^{3}	1.74±0.44
Cd ²⁺	1.45(73)	-4438(1759)	12	0.39	38±6 (ppb) ¹	12±2.4 (ppb) ³	2.12±0.43
ln ^{3+ d}	_	_	-	_	13±2 ¹	1.66±0.69 ³	2.65±0.37
Sn ²⁺	-1.42(71)	4498(1696)	20	0.44	118±19 ¹	39±8 ³	2.10±0.44
Ge ²⁺	-1.38(56)	8040(1433)	9	0.82	1140±120 ¹	15±3 ³	3.68±0.33
Pb ²⁺	1.47(39)	-3370(957)	19	0.42	167±14 ¹	28±6 ³	2.51±0.35
Se	-3.23(29)	10982(583)	36	0.91	80±17 ⁵	24±5 ³	2.17±0.41
Те	–2.95(37)	10891(725)	36	0.87	11±1.7 ⁵	4.1 ± 0.8^{3}	2.04±0.40

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References: [1] Wang et al. (2018) [2] Sossi et al. (2018) [3] Hauri et al. (2015) [4] Delano (1986) [5] Wang and Becker (2013) a Low R² reflects an absence of temperature effects (i.e., the variability of elemental metal-silicate partitioning is predominantly explained by variability in fO2) and is not indicative of overall scatter of D values ^b Assuming a 20 % 734 uncertainty on lunar mantle estimates of Co, Cu, Zn, Cd, In, Sn, Ge, Ga, Pb, Se, Te as no uncertainties were reported in Hauri et al. (2015) ° Calculated using Eq. (4) ^d The siderophile behavior of In and Ga is unaffected by temperature within the studied range – for modelling we therefore assumed $D_{Ga}^{met \, liq-sil \, melt} = 3$ and $D_{In}^{met \, liq-sil \, melt} = 10$ (Table 735 736 1).















Supplementary information file for "A possible high-temperature origin of the Moon and its geochemical consequences" by E.S. Steenstra, J. Berndt, S. Klemme, Y. Fei and W. van Westrenen.

A.1 Quantification of run temperatures using power-*T* curves

At the pressures relevant for lunar core formation tungsten-rhenium thermocouples melt at ~2500 K. We therefore constrained the experimental run temperatures at temperatures that exceed the melting point of the thermocouple using well-defined power-temperature relationships, obtained at temperatures below the thermocouple melting point. For Cr-doped MgO octahedra at a hydraulic pressure of 109 bar (equivalent to a sample pressure of 3.8 GPa), experimental temperatures are calculated as a function of power (in Watts) using the following relationship (based on three experiments):

$$T(^{\circ}C) = 1.94 * \text{power}(W) - 109$$
 (*R*² = 0.99) (A.1)

For runs for which ZrO_2 octahedra were used, power-T curves yield (based on 16 experiments):

$$T(^{\circ}C) = 2.41 * \text{power (W)} - 93$$
 (A.2) (A.2)

Based on the variability in power-temperature relationships illustrated in Fig. S.1 we calculate an estimated uncertainty of ~50 K on calculated run temperatures for experiments performed in ZrO_2 octahedra and ~100 K for experiments performed in Cr-doped MgO octahedra (see main-text Table 1).

A.2 Details of EPMA analyses of experimental run products

Major and trace element concentrations in the run products were obtained using electron microprobes at the Institute of Mineralogy at the University of Munster and at the Dutch National Geological Facility at Utrecht University. Both institutes are equipped with a JEOL JXA 8530F field emission electron microprobe. Measurement points were set in lines and/or raster grids, depending of the available surface area of the analysed phases. The electron beam size was approximately equivalent to the step size (5–15 um), while using a beam current of 15 nA and an accelerating voltage of 15 kV. Dwell times of 20–30 s on peak and 10–15 s on each background were used. At least 20 repeat analyses were performed if sufficient sample surface area was available, and usually more (N > 30). Care was taken to avoid analyses of areas close to the edge of phases and/or surrounding capsule materials. Standards used for metal analyses were KTiPO5 or apatite for P, fayalite or pure Fe metal for Fe, TiO₂ or rutile for Ti, tephroite or rhodonite for Mn, pure metal or willemite for Zn, galena or Pb-Zn glass for Pb, pure

metal or InAs for In, GaAs or InAs for As, pure metal or CdS for Cd, hypersthene or diopside for Si, chalcopyrite or pyrite for S, pure metal or Cr_2O_3 for Cr, pure metal or NiO for Ni, and pure metal standards for V, Co, Cu, Ge, Se, Sn, Sb, Te, Mo and W. Elements Na, Si, Al, Se, Mg, As and Ge were measured on the TAP crystal; Ca, P, S, Mo, Sb, Cd, K, Sn, Ti on the PETJ crystal; V, Cr, Mn, Fe, Co, Ni, Cu, W, Zn on the LIFL crystal and Pb, Bi, In, Te on the PETH crystal.

Silicate melt reference materials for major and minor elements were diopside for Si, diopside for Ca, forsterite for Mg, corundum for Al, hematite for Fe, tephroite or MnO₂ for Mn, KTiPO₅ or orthoclase for K, GaP or KTiPO₅ for P, TiO₂ for Ti, jadeite for Na, galena for Pb, CdTe for Cd and Te, InAs for In, chalcopyrite or pyrite for S, and pure metal reference materials for Cr, Ni, Se, Cu, Zn and Sn. Calibrations were considered successful when the primary standard compositions were reproduced within 1% relative deviation. In Steenstra et al. (2019) we present a full analysis of the accuracy of our analytical strategy, using analyses of the NIST 610 reference glass with the EPMA standardization that was implemented in the previous studies that are used in this work. We observed that there is generally good agreement (i.e. within 10% relative deviation) between reference and measured values, despite the low ,concentrations of nominally 500 ppm and the use of a moderate beam current of 15 nA due to the beam sensitive nature of silicate glasses (Fig. S.3). Several analyses of the NIST 616 glass, that contains approximately 0.5 ppm of each trace element, were also performed to assess true zero counts for the elements of interest and confirmed the accuracy and precision of our analytical approach.

A.3 Corrections for matrix effects for LA-ICP-MS analyses of Fe-rich alloys

We have recently shown that the use of non-matrix matched silicate reference materials for analyses of volatile or highly refractory trace elements in Fe-rich metals may result in erroneous results (Steenstra et al., 2019). Although this issue does not affect the results discussed in this study due to the fact that the elements considered here are non-volatile it does affect the concentrations determined for other volatile and highly refractory trace elements in the metal alloys. To address this issue, we derived empirical correction terms by comparison of trace element measurements obtained by EPMA and LA-ICP-MS (Steenstra et al., 2019). We use the correction terms from the latter study to correct for the matrix effects.

A.4 Compositional effects on metal-silicate partitioning behavior of Mo and W The metal-silicate partitioning behavior of Mo and W, like P, is strongly affected by variabilities in silicate melt composition (e.g. O'Neill and Eggins, 2002; Righter et al., 2010; Siebert et al., 2011; Steenstra et al., 2017). Given the strong correlation between increasing temperatures and increasing interaction of the silicate melt with the MgO capsule (Fig. S.4), observed temperature trends for Mo and W could be partly and/or fully the result of variations in silicate melt composition. Unfortunately, the exact effects of each of the major element oxide on activities of Mo and W in the silicate melt are not well constrained and *cannot* be described using a single silicate compositional parameter such as nbo/t (O'Neill and Eggins, 2002) prohibiting a quantitative analysis of the effects of *T* on Mo and W metal-silicate partitioning. However, the individually determined $D_W^{met \, liq - sil \, melt}$ values should be representative of that of lunar metal-silicate equilibrium. This is justified by the similar CaO contents of the bulk silicate Moon and those of the experimental silicate melts produced in the highest-*T* experiments, as it has been shown that $D_W^{met \, liq - sil \, melt}$ most strongly varies as a function of CaO (O'Neill and Eggins, 2002; Steenstra et al., 2017).

A.5 Metal-silicate partitioning of W during high-T lunar differentiation

Thiemens et al. (2019) recently studied the Hf/W ratio of the Moon and suggested that a $D_W^{met \, liq-sil \, melt}$ value of 60 would be required to explain the present-day Hf/W ratio of the lunar mantle. A temperature effect on $D_W^{met \, liq-sil \, melt}$ could unfortunately not be derived in this study for lunar compositions due to strong correlations of silicate melt composition and temperature (Fig. S.4). The lack of a temperature effect on $\log K_W$ for lunar melt compositions observed in this study could suggest that the temperature dependence of $\log D_w$ is indistinguishable from that of $\log D_{Fe}$. In any case, the $\log D_w$ values measured for the highest temperature experiments (possessing similar silicate melt compositions and obtain within the range of proposed core formation temperatures) are consistent with the proposed Hf/W ratio of the silicate Moon for a 1.5% lunar core mass, showing that high-temperature core formation (as inferred from Ni and Co systematics) would reproduce the Hf/W of the lunar mantle (Fig. S.5; Thiemens et al., 2019).

A.6 Potential effects of late veneer on volatile siderophile/chalcophile element abundances in the lunar mantle

To illustrate the potential effects of a lunar late veneer on volatile siderophile and chalcophile element abundances, we assumed a 0.02 to 0.05 mass% (Kruijer et al., 2015) contribution of CI chondrites (the most volatile siderophile- and chalcophile element meteorite suite) or H chondrites to the lunar mantle, while using the bulk compositional estimates of Alexander (2019) and Newsom (1995) and references therein. The results suggests that the majority of the lunar mantle abundances (except of Ge and to a lesser extent Se and Te) would remain unaffected by a late veneer, especially given the likely degassing of such elements following impact.

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Fig. S.1 Power temperature relationships derived from experiments performed using thermocouples for experiments conducted using Cr-doped MgO octahedra (left) and ZrO₂ octahedra (right).



Fig. S.2 Comparison between measured and reported trace elements (GeoRem database, Application Version 19 and references therein) determined for NIST-610 and GSD-1G using different beam sizes (from Steenstra et al. 2019, but measured in between sessions in which samples from this study were analysed).



Fig. S.3 Relative deviations between reference concentrations of silicate reference material NIST 610 (taken from the GeoRem database website) and those measured by electron microprobe in this study. Shaded area represents the range of published data, dotted lines define 10% relative deviation. All uncertainties are 1 standard deviation (figure from Steenstra et al. 2019, but measured in between sessions in which samples from this study were analysed).



Fig. S.4 Correlation between experimental peak temperature and abundance of major element oxides in the silicate melt. Crosses indicate initial major oxide concentrations prior to experiment.

Figure S.5 Log $D_W^{\text{met liq-sil melt}}$ values from this study as a function of temperature. Values were normalized to a lunar *f*O₂ of 2 units below the iron-wüstite buffer (Steenstra et al., 2016) assuming a valence state of 6+ for W (Siebert et al., 2011). Horizontal line indicates the minimum estimate of log $D_W^{\text{met liq-sil melt}}$ during lunar core formation required for explaining the Hf/W ratio of the silicate Moon (Thiemens et al., 2019).

Run #	PR1446	PR1449	PR1450	PR1465	PR1468	PR1470	PR1477	PR1480	PR1481	PR1489	PR1491	PR1505	PR1506	PR1508
	$N = 35^{\circ}$	$\frac{N=29}{45.05(00.4)}$	N = 32	N = 29	N = 30	N = 00	N = 20	N = 19	N = 30	N = 30	N = 07	N = 13	N = 24	N = 10
SiO	39.08(271)	45.25(264)	47.42(110)	49.75(197)	32.23(150)	44.23(200)	46.66(192)	46.21(195)	45.02(122) 36.65(62)	51.04(359) 33.59(266)	61.79(187) 25.41(194)	50.00(174) 31.80(243)	54.40(213) 26.65(187)	63.97(139) 24.07(142)
	7 58(119)	4 99(111)	4 05(76)	2 60(142)	7 31(54)	4 14(102)	4 75(145)	4 15(95)	4 90(70)	3 28(136)	2 60(36)	3 79(80)	3 72(52)	3.26(24)
CaO	8 65(154)	6.02(167)	4 76(73)	3 54(130)	7 46(67)	5 43(133)	3 93(87)	5 39(112)	5 56(68)	4 27(221)	3 10(47)	4 70(104)	3 61(49)	3 68(32)
FeO	7.80(68)	4.30(49)	4.55(41)	4.56(62)	8.78(14)	7.37(87)	6.05(67)	6.19(89)	5.89(34)	4.83(81)	4.56(41)	7.19(87)	7.28(57)	4.97(28)
K ₂ O	0.014(5)	0.01(1)	0.03(1)	0.006(3)	0.023(3)	0.01(1)	0.009(3)	0.02(1)	0.010(3)	0.02(1)	0.010(2)	0.006(3)	0.03(1)	n.d.
Na ₂ O	0.03(1)	0.03(1)	0.61(13)	0.31(13)	0.08(1)	0.05(1)	0.016(5)	0.65(12)	0.15(7)	0.08(1)	0.61(11)	0.29(7)	1.51(29)	n.d.
MnO	0.18(2)	0.14(1)	0.10(1)	0.06(1)	0.19(1)	0.74(7)	0.12(1)	0.10(1)	1.00(6)	0.09(1)	0.049(4)	0.85(6)	0.66(2)	0.07(3)
Cr ₂ O ₃	0.24(2)	0.16(2)	0.10(2)	0.05(3)	0.30(1)	0.65(13)	0.21(4)	0.12(3)	0.83(10)	0.09(3)	0.07(1)	0.73(15)	0.71(8)	0.13(3)
V ₂ O ₃	-	-	-	-	-	0.68(13)	-	-	0.92(10)	-	-	1.28(25)	0.75(7)	-
TiO₂	0.24(4)	0.16(4)	0.13(2)	0.07(3)	0.21(1)	0.15(4)	0.13(3)	0.14(3)	0.14(2)	0.11(4)	0.06(1)	0.11(2)	0.10(2)	0.09(1)
NiO	0.01(1)	0.008(4)	0.02(1	0.007(3)	0.009(4)	0.011(3)	0.01(1)	0.01(1)	0.011(5)	0.02(1)	0.010(3)	0.007(4)	0.01(1)	0.01(1)
CoO	-	-	-	-	-	0.02(1)	-	-	0.012(4)	-	-	0.02(1)	0.03(1)	-
P ₂ O ₅	-	-	-	-	-	0.06(2)	-	-	0.03(1)	- 	-	0.06(2)	0.06(2)	-
In ₂ O ₃	0.11(2)	0.11(2)	0.10(2)	0.06(2)	0.11(1)	-	0.08(1)	0.06(2)	-	n.d. "	0.09(1)	-	-	0.10(1)
CdO	0.24(5)	0.08(2)	0.11(4)	0.03(1)	0.30(3)	-	0.06(2)	0.06(5)	-	0.09(9)	0.07(2)	-	-	n.d.
5002	0.07(3)	0.01(1)	0.00(3)	0.03(2)	0.004(3)	-	D.0.1.*	0.20(8)	-	0.19(18) n.d	0.75(12)	-	-	0.37(7)
PhO	0.002(2)	0.03(1)	0.02(1)	0.000(4)	0.002(2) 0.15(2)	_	0.03(2)	0.24(3)	_	0.04(3)	0.23(3)	_	_	0.01(2) 0.02(1)
SO.	0.09(3)	0.03(1)	0.00(2)	0.02(2) 0.02(1)	0.13(2) 0.20(7)	- 0.012(3)	0.03(2)	0.03(2)	 0.01(1)	0.04(3)	0.03(1)	– hdl	_ 0.01(1)	0.02(1) 0.004(3)
ZrO ₂	0.01(1)	0.008(4)	0.10(0) 0.24(4)	0.02(1)	0.20(7) 0.14(1)	0.012(0)	0.04(1)	0.01(1)	0.05(1)	bdl ^c	0.10(0)	0.05(2)	0.01(1) 0.02(1)	n d
Total	99.45(28)	100.06(29)	99.34(35)	99.28(42)	100.56(15)	97.75(28)	99.97(25)	99.34(50)	101.24(26)	97.78(53)	99.62(35)	100.96(42)	99.61(53)	101.64(22)
LA-ICP-MS	N = 13	N = 9	N=25	N = 5	N = 10	N = 13	N = 8	N = 8	N = 11	N = 13	N = 12	N = 10	N = 11	N = 11
	-	-	-	-	-	N (P) = 7	-	-	N (P) = 9	-	-	N(P) = 6	N (P) = 7	-
CaO (wt.%)	7.62(63)	6.86(78)	5.42(24)	4.87(123)	8.69(14)	5.76(26)	6.31(104)	4.68(37)	6.19(29)	4.51(15)	3.24(29)	5.32(23)	3.56(11)	3.64(13)
Ti (ppm)	1378(86)	1190(124)	953(40)	704(207)	1467(20)	906(34)	1052(167)	751(51)	969(42)	706(33)	526(39)	832(33)	581(17)	613(21
P	-	-	-	-	-	117(7)	-	-	154(27)	-	-	197(11)	223(12)	-
V	-	_	_	_	_	5010(158)	_	_	6640(212)	-	_	9836(427)	5045(203)	-
Cr	1518(38)	1176(73)	651(35)	298(86)	2193(28)	4949(155)	1475(95)	916(136)	5718(195)	627(57)	737(93)	5335(235)	4585(216)	647(37)
Mn	1354(62)	1213(65)	838(25)	518(100)	1583(6)	6024(156)	1175(114)	809(48)	7977(246)	744(29)	518(39)	7061(211)	4870(102)	541(16)
CO Ni	-	-	- 71(11)	- 29(12)	-	93(4)	- 64(4)	- 70(17)	41(4)	- 76(11)	-	84(4)	113(4) 54(2)	-
	43(2)	22(1)	7 I(II) 2 5(7)	30(12)	S7(1) 6 6(0)	3Z(Z)	17(4)	2 3(6)	0.62(8)	70(11) 2 7(4)	2 8(7)	33(2)	1 9(2)	120(21)
Zn	1.20(21)	13(1)	12(6)	2.0(2)	32(1)	2.7(2) 20(1)	20(2)	2.3(0) 14(1)	18(7)	2.7(4) 6.9(5)	13(2)	1.34(17)	13(1)	2.3(7)
Ga	1 26(11)	1 45(12)	1 13(8)	18(7)	1 6(1)	1 11(6)	1.30(22)	0.73(6)	0.92(8)	0.60(4)	0.68(11)	1 17(10)	0 74(5)	0.56(5)
Ge	-	-	_	-	_	21(1)	-	-	5.9(23)	-	-	29(3)	45(4)	-
As	b.d.l.	2.0(8)	2.4(5)	9.7(43)	2.0(5)	_	2.9(2)	5.2(6)	_	1.83(19)	4.4(8)	_	_	10(4)
Se	673(44)	519(52)	925(44)	510(102)	321(7)	-	484(69)	965(123)	_	1761 (151)	3813(904)	-	-	2638(193)
Zr	665(48)	56(6)	1846(115)	2883(1042)	979(25)	215(10)	337(57)	55(3)	357(21)	57(2)	155(11)	317(14)	61(12)	52(3)
Мо	-	-	-	-	_	13(2)	-	-	11(2)	-	-	28(2)	47(4)	-
Cd	2338(203)	1689(168)	1503(145)	665(132)	3467(65)	-	1607(207)	1013(200)	-	998(64)	1263(165)	-	-	1085(107)
In	948(71)	1506(145)	1004(125)	912(190)	966(12)	-	936(138)	732(130)		494(39)	1095(213)	-	-	768(127)
Sn	0.15(2)	0.30(4)	0.22(5)	b.d.l.	0.17(4)	0.15(3)	0.36(6)	<0.24	b.d.l.	<0.08(1)	0.31(7)	0.11(2)	0.14(3)	<0.09(1)
Sb	3.3(5)	3.3(7)	16(3)	4.3(36)	1.25(10)	-	24(4)	21(4)	-	6.0(15)	3.8(10)	-	-	26(8)
Te	206(15)	74(6)	427(51)	150(35)	63(2)	-	122(15)	1699(279)	-	524(57)	2197(510)	_	_	1168(212)
W	-	-	-	-	- 1556(10)	141(14)	-	-	81(8)	-	-	91(11)	163(26)	-
	950(102)	629(90)	005(90)	201(37)	1000(19)	0.28(3)	009(04)	303(70)	0.30(5)	320(42)	344(44)	0.30(3)	0.16(2)	401(115)
Run #	PR1510	PR1517	PR1518	PR1521	PR1522	PR1524	PR1538	PR1539	PR1561					
	N = 20	11 = 29	N = 29	11 = 33	IN = 30	N = 20	IN = 3U	N = 29	10 = 25					

Table S.1 Silicate compositions of experimental charges determined by EPMA and LA-ICP-MS.

MgO	54.22(170)	65.10(209)	53.80(127)	56.95(209)	46.63(134)	62.70(240)	23.72(120)	45.17(143)	21.46(77)
SiO ₂	28.48(185)	18.44(226)	29.19(156)	25.76(242)	36.38(96)	21.76(213)	36.47(61)	34.41(123)	44.19(51)
Al ₂ O ₃	3.97(57)	2.87(31)	3.84(50)	3.23(41)	4.88(88)	3.20(48)	8.52(49)	4.48(90)	9.73(52)
CaO	4.61(70)	2.65(48)	4.42(59)	4.43(63)	6.20(89)	3.23(38)	11.82(76)	5.91(75)	12,19(39)
FeO	7 13(58)	9 13(58)	7 66(50)	7 40(59)	5 49(46)	7 58(37)	11 96(44)	7 56(64)	10.02(52)
K-0	0.008(4)	0.003(2)	0.007(2)	0.004(2)	0.009(3)	0.002(1)	0.012(2)	0.004(2)	0.007(3)
Na.O	0.000(4)	0.000(2)	0.007(2)	0.00+(2)	0.000(0)	0.002(1)	0.030(5)	0.00+(2) 0.03(1)	0.007(0)
MnO	0.10(0)	0.01(1)	0.50(7)	0.64(2)	0.02(1)	0.06(1)	2,00(8)	1 14(6)	0.017(+) 0.22(1)
Cr.O.	0.04(3)	0.34(1)	0.59(2)	0.04(2)	0.12(1) 0.12(2)	0.00(1)	2.09(0)	0.97(16)	0.23(1)
	0.71(9)	0.04(3)	0.02(0)	0.01(7)	0.13(3)	0.11(1)	1.94(10)	0.07(10)	0.47(2)
V2U3	0.75(9)	0.73(4)	0.00(0)	0.71(7)	-	-	2.06(14)	1.01(16)	-
	0.12(2)	0.08(1)	0.12(2)	0.10(1)	0.17(2)	0.08(1)	0.30(2)	0.15(3)	0.30(2)
NIO	0.02(1)	0.02(1)	0.013(5)	0.013(4)	0.02(1)	0.015(5)	0.008(4)	0.008(3)	0.01(1)
C00	0.02(1)	0.05(1)	0.03(1)	0.03(1)	-	-	0.02(1)	0.02(1)	-
P ₂ O ₅	0.02(1)	0.01(1)	0.02(1)	0.01(1)	-	-	0.06(1)	0.03(1)	-
In ₂ O ₃	-	-	-	-	0.04(1)	0.05(1)	-	-	0.09(1)
CdO	-	-	-	-	0.08(3)	0.05(2)	-	-	0.48(3)
SeO2	-	-	-	-	0.15(5)	0.16(6)	-	-	0.005(4)
TeO2	-	-	-	-	0.01(1)	0.04(2)	-	-	b.d.l.
PbO	-	-	-	-	0.03(1)	0.02(1)	-	-	0.13(3)
SO₃	0.02(1)	0.01(1)	0.009(4)	0.01(1)	0.01(1)	0.013(5)	0.009(4)	0.01(1)	0.01(1)
ZrO ₂	0.06(2)	0.03(1)	0.01(1)	0.02(1)	0.04(1)	0.02(1)	0.13(2)	0.05(2)	0.17(2)
Total	101.00(44)	100.39(32)	101.10(21)	100.00(22)	100.40(19)	99.11(41)	99.23(16)	100.93(26)	99.53(11)
LA-ICP-MS	N – 15	N – 11	N – 12	N - 12	N - 10	N - 3	N - 10	N - 10	N - 14
					11 = 10	11=0			
	N(P) = 10	N(P) = 7	N(P) = 7	N(P) = 0	-	_	N(P) = 7	N(P) = 8	-
0-0 (N(P) = 10	N(P) = 7	N(P) = 7	N(P) = b	-	-	N(P) = 7	N(P) = 8	-
CaO (wt.%)	N(P) = 10 4.74(11)	N(P) = 7 2.60(18)	N(P) = 7 4.91(15)	N(P) = 6 4.13(15)	4.99(22)	 3.11(34)	N(P) = 7 12.88(59)	N(P) = 8 5.24(30)	11.95(18)
CaO (wt.%) Ti (ppm)	N(P) = 10 4.74(11) 818(20)	N(P) = 7 2.60(18) 442(21)	N(P) = 7 4.91(15) 823(27)	$ \begin{array}{l} $	- 4.99(22) 825(28)	– 3.11(34) 504(54)	N(P) = 7 12.88(59) 2080(84)	N(P) = 8 5.24(30) 864(36)	 11.95(18) 1959(50)
CaO (wt.%) Ti (ppm) P	$\frac{N(P) = 10}{4.74(11)}$ 818(20) 77(4) 5525(240)	N(P) = 7 2.60(18) 442(21) 60(5)	<u>N(P) = 7</u> 4.91(15) 823(27) 102(6)	4.13(15) 669(17) 85(11)	- 4.99(22) 825(28) -	_ 3.11(34) 504(54) _	N(P) = 7 12.88(59) 2080(84) 226(20)	N (P) = 8 5.24(30) 864(36) 126(6)	
CaO (wt.%) Ti (ppm) P V	N(P) = 10 4.74(11) 818(20) 77(4) 5372(218)	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644)	N(P) = 7 4.91(15) 823(27) 102(6) 5243(225)	N(P) = 6 4.13(15) 669(17) 85(11) 6333(535)	- 4.99(22) 825(28) - -		N(P) = 7 12.88(59) 2080(84) 226(20) 14875(652)	N (P) = 8 5.24(30) 864(36) 126(6) 7126(321)	
CaO (wt.%) Ti (ppm) P V Cr	N(P) = 10 4.74(11) 818(20) 77(4) 5372(218) 4782(209)	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668)	N(P) = 7 4.91(15) 823(27) 102(6) 5243(225) 4712(219)	N(P) = 6 4.13(15) 669(17) 85(11) 6333(535) 5212(490) 5212(490)	- 4.99(22) 825(28) - 972(98)		N(P) = 7 12.88(59) 2080(84) 226(20) 14875(652) 12230(570)	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259)	- 11.95(18) 1959(50) - - 3339(63)
CaO (wt.%) Ti (ppm) P V Cr Mn	N(P) = 10 4.74(11) 818(20) 77(4) 5372(218) 4782(209) 5013(128)	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971)	N(P) = 7 4.91(15) 823(27) 102(6) 5243(225) 4712(219) 5011(108)	N(P) = 6 4.13(15) 669(17) 85(11) 6333(535) 5212(490) 5664(365)	- 4.99(22) 825(28) - - 972(98) 853(32)	_ 3.11(34) 504(54) _ _ 690(18) 506(46)	N(P) = 7 12.88(59) 2080(84) 226(20) 14875(652) 12230(570) 16696(549)	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222)	
CaO (wt.%) Ti (ppm) P V Cr Mn Co	N (P) = 10 4.74(11) 818(20) 77(4) 5372(218) 4782(209) 5013(128) 98(4)	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19)	N(P) = 7 4.91(15) 823(27) 102(6) 5243(225) 4712(219) 5011(108) 150(6)	N(P) = 6 4.13(15) 669(17) 85(11) 6333(535) 5212(490) 5664(365) 209(17)	- 4.99(22) 825(28) - 972(98) 853(32) -		N(P) = 7 12.88(59) 2080(84) 226(20) 14875(652) 12230(570) 16696(549) 71(3)	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5)	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni	$\begin{array}{c} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2) \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10)	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \end{array}$	$\begin{array}{c} N(P) = 6\\ 4.13(15)\\ 669(17)\\ 85(11)\\ 6333(535)\\ 5212(490)\\ 5664(365)\\ 209(17)\\ 108(8) \end{array}$	- 4.99(22) 825(28) - 972(98) 853(32) - 46(5)	- 3.11(34) 504(54) - 690(18) 506(46) - 250(78)	$\begin{array}{c} N\left(P\right)=7\\ 12.88(59)\\ 2080(84)\\ 226(20)\\ 14875(652)\\ 12230(570)\\ 16696(549)\\ 71(3)\\ 12(1) \end{array}$	$\frac{N(P) = 8}{5.24(30)}$ $\frac{5.24(30)}{864(36)}$ $\frac{126(6)}{7126(321)}$ $\frac{5853(259)}{8594(222)}$ $\frac{94(5)}{33(2)}$	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu	$\begin{array}{l} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3) \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17)	N(P) = 7 4.91(15) 823(27) 102(6) 5243(225) 4712(219) 5011(108) 150(6) 71(4) 1.8(1)	$\frac{N(P) = 6}{669(17)}$ $\frac{4.13(15)}{669(17)}$ $\frac{85(11)}{6333(535)}$ $5212(490)$ $5664(365)$ $209(17)$ $108(8)$ $1.9(1)$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3)	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12)	$\begin{array}{l} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \end{array}$	N (P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5) 33(2) 0.80(12)	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn	N(P) = 10 4.74(11) 818(20) 77(4) 5372(218) 4782(209) 5013(128) 98(4) 45(2) 2.3(3) 14(1)	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17)	N(P) = 7 4.91(15) 823(27) 102(6) 5243(225) 4712(219) 5011(108) 150(6) 71(4) 1.8(1) 17(1)	$\frac{N(P) = 6}{669(17)}$ $\frac{4.13(15)}{669(17)}$ $\frac{85(11)}{6333(535)}$ $5212(490)$ $5664(365)$ $209(17)$ $108(8)$ $1.9(1)$ $12(1)$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1)	- 3.11(34) 504(54) - 690(18) 506(46) - 250(78) 6.1(12) 11(1)	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \end{array}$	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5) 33(2) 0.80(12) 14.4(4)	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga	N(P) = 10 4.74(11) 818(20) 77(4) 5372(218) 4782(209) 5013(128) 98(4) 45(2) 2.3(3) 14(1) 1.15(6)	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4)	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3)	- 3.11(34) 504(54) - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11)	$\begin{array}{c} N\left(P\right)=7\\ 12.88(59)\\ 2080(84)\\ 226(20)\\ 14875(652)\\ 12230(570)\\ 16696(549)\\ 71(3)\\ 12(1)\\ 2.0(2)\\ 37(2)\\ 1.7(1) \end{array}$	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5) 33(2) 0.80(12) 14.4(4)	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge	$\begin{array}{l} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3)\\ 14(1)\\ 1.15(6)\\ 30(1) \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7)	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \end{array}$	$\begin{array}{c} N(P) = 6\\ 4.13(15)\\ 669(17)\\ 85(11)\\ 6333(535)\\ 5212(490)\\ 5664(365)\\ 209(17)\\ 108(8)\\ 1.9(1)\\ 12(1)\\ 0.65(4)\\ 57(4) \end{array}$	- 4.99(22) 825(28) - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) -	- 3.11(34) 504(54) - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) -	$\begin{array}{c} N\left(P\right)=7\\ 12.88(59)\\ 2080(84)\\ 226(20)\\ 14875(652)\\ 12230(570)\\ 16696(549)\\ 71(3)\\ 12(1)\\ 2.0(2)\\ 37(2)\\ 1.7(1)\\ 3.8(4) \end{array}$	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5) 33(2) 0.80(12) 14.4(4) 19(1)	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As	$\begin{array}{c} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3)\\ 14(1)\\ 1.15(6)\\ 30(1)\\ -\end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7) -	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \end{array}$	$\begin{array}{c} N(P) = 6\\ 4.13(15)\\ 669(17)\\ 85(11)\\ 6333(535)\\ 5212(490)\\ 5664(365)\\ 209(17)\\ 108(8)\\ 1.9(1)\\ 12(1)\\ 0.65(4)\\ 57(4)\\ -\end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l.	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.777(11) - 7.1(24)	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \end{array}$	$\begin{array}{l} N(P) = 8 \\ 5.24(30) \\ 864(36) \\ 126(6) \\ 7126(321) \\ 5853(259) \\ 8594(222) \\ 94(5) \\ 33(2) \\ 0.80(12) \\ 14.4(4) \\ 19(1) \\ - \end{array}$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l.
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se	$\begin{array}{c} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3)\\ 14(1)\\ 1.15(6)\\ 30(1)\\ -\\ -\end{array}$	$\begin{array}{c} N(P) = 7 \\ 2.60(18) \\ 442(21) \\ 60(5) \\ 4660(644) \\ 3875(668) \\ 5259(971) \\ 159(19) \\ 83(10) \\ 1.27(17) \\ 9.6(17) \\ 0.44(4) \\ 50(7) \\ - \\ - \end{array}$	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ - \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105)	- 3.11(34) 504(54) - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354)	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \\ - \end{array}$	$\begin{array}{c} N\left(P\right) = 8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ -\end{array}$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr	$\begin{array}{l} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3)\\ 14(1)\\ 1.15(6)\\ 30(1)\\ -\\ -\\ 414(20) \end{array}$	$\begin{array}{c} N(P) = 7 \\ 2.60(18) \\ 442(21) \\ 60(5) \\ 4660(644) \\ 3875(668) \\ 5259(971) \\ 159(19) \\ 83(10) \\ 1.27(17) \\ 9.6(17) \\ 0.44(4) \\ 50(7) \\ - \\ 211(14) \end{array}$	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ 44(2) \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ 58(2) \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8)	- 3.11(34) 504(54) - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13)	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \\ 934(36) \end{array}$	$\begin{array}{c} N\left(P\right) = 8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ 301(15)\\ \end{array}$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8) 1246(49)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr Mo	$\begin{array}{c} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3)\\ 14(1)\\ 1.15(6)\\ 30(1)\\ -\\ -\\ 414(20)\\ 19(1)\\ \end{array}$	$\begin{array}{c} N(P) = 7 \\ 2.60(18) \\ 442(21) \\ 60(5) \\ 4660(644) \\ 3875(668) \\ 5259(971) \\ 159(19) \\ 83(10) \\ 1.27(17) \\ 9.6(17) \\ 0.44(4) \\ 50(7) \\ - \\ - \\ 211(14) \\ 40(5) \end{array}$	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \\ 58(2) \\ 43(3) \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) -	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) -	$\begin{array}{c} N\left(P\right)=7\\ 12.88(59)\\ 2080(84)\\ 226(20)\\ 14875(652)\\ 12230(570)\\ 16696(549)\\ 71(3)\\ 12(1)\\ 2.0(2)\\ 37(2)\\ 1.7(1)\\ 3.8(4)\\ -\\ -\\ 934(36)\\ 21(4) \end{array}$	$\begin{array}{c} N\left(P\right) = 8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ 301(15)\\ 13(1)\\ \end{array}$	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr Mo Cd	$\begin{array}{c} N\left(P\right) = 10\\ 4.74(11)\\ 818(20)\\ 77(4)\\ 5372(218)\\ 4782(209)\\ 5013(128)\\ 98(4)\\ 45(2)\\ 2.3(3)\\ 14(1)\\ 1.15(6)\\ 30(1)\\ -\\ -\\ 414(20)\\ 19(1)\\ -\\ -\end{array}$	$\begin{array}{c} N(P) = 7 \\ 2.60(18) \\ 442(21) \\ 60(5) \\ 4660(644) \\ 3875(668) \\ 5259(971) \\ 159(19) \\ 83(10) \\ 1.27(17) \\ 9.6(17) \\ 0.44(4) \\ 50(7) \\ - \\ - \\ 211(14) \\ 40(5) \\ - \end{array}$	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \\ - \\ - \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55)		$\begin{array}{c} N\left(P\right)=7\\ 12.88(59)\\ 2080(84)\\ 226(20)\\ 14875(652)\\ 12230(570)\\ 16696(549)\\ 71(3)\\ 12(1)\\ 2.0(2)\\ 37(2)\\ 1.7(1)\\ 3.8(4)\\ -\\ -\\ 934(36)\\ 21(4)\\ -\end{array}$	$\begin{array}{l} N(P) = 8 \\ 5.24(30) \\ 864(36) \\ 126(6) \\ 7126(321) \\ 5853(259) \\ 8594(222) \\ 94(5) \\ 33(2) \\ 0.80(12) \\ 14.4(4) \\ 19(1) \\ - \\ - \\ 301(15) \\ 13(1) \\ - \\ - \end{array}$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8) 1246(49) - 5158(238)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr Mo Cd In	$\begin{array}{c} N\left(P\right) = 10 \\ 4.74(11) \\ 818(20) \\ 77(4) \\ 5372(218) \\ 4782(209) \\ 5013(128) \\ 98(4) \\ 45(2) \\ 2.3(3) \\ 14(1) \\ 1.15(6) \\ 30(1) \\ - \\ - \\ 414(20) \\ 19(1) \\ - \\ - \\ b.d.l. \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7) 211(14) 40(5) - 0.61(5)	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \\ - \\ 1.22(12) \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ - \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55) 311(20)	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) - 1470(437) 1012(226)	$\begin{array}{c} N\left(P\right)=7\\ 12.88(59)\\ 2080(84)\\ 226(20)\\ 14875(652)\\ 12230(570)\\ 16696(549)\\ 71(3)\\ 12(1)\\ 2.0(2)\\ 37(2)\\ 1.7(1)\\ 3.8(4)\\ -\\ -\\ 934(36)\\ 21(4)\\ -\\ -\\ -\end{array}$	$\begin{array}{c} N\left(P\right)=8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ 301(15)\\ 13(1)\\ -\\ -\\ -\\ \end{array}$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8) 1246(49) - 5158(238) 941(52)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ga Ga Ga Se Zr Mo Cd In Sn	$\begin{array}{l} N(P) = 10 \\ 4.74(11) \\ 818(20) \\ 77(4) \\ 5372(218) \\ 4782(209) \\ 5013(128) \\ 98(4) \\ 45(2) \\ 2.3(3) \\ 14(1) \\ 1.15(6) \\ 30(1) \\ - \\ - \\ 414(20) \\ 19(1) \\ - \\ b.d.l. \\ 0.13(1) \end{array}$	$\begin{array}{c} N(P) = 7 \\ 2.60(18) \\ 442(21) \\ 60(5) \\ 4660(644) \\ 3875(668) \\ 5259(971) \\ 159(19) \\ 83(10) \\ 1.27(17) \\ 9.6(17) \\ 0.44(4) \\ 50(7) \\ - \\ 211(14) \\ 40(5) \\ - \\ 0.61(5) \\ b.d.l. \end{array}$	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \\ - \\ 1.22(12) \\ b.d.l. \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ b.d.l. \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55) 311(20) 0.11(1)	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) - 1470(437) 1012(226) b.d.l.	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \\ - \\ 934(36) \\ 21(4) \\ - \\ - \\ b.d.l. \end{array}$	$\begin{array}{c} N\left(P\right) = 8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ 301(15)\\ 13(1)\\ -\\ -\\ b.d.l.\\ \end{array}$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8) 1246(49) - 5158(238) 941(52) 0.16(3)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr Mo Cd In Sn Sb	$\begin{array}{c} N\left(P\right) = 10 \\ 4.74(11) \\ 818(20) \\ 77(4) \\ 5372(218) \\ 4782(209) \\ 5013(128) \\ 98(4) \\ 45(2) \\ 2.3(3) \\ 14(1) \\ 1.15(6) \\ 30(1) \\ - \\ - \\ 414(20) \\ 19(1) \\ - \\ b.d.l. \\ 0.13(1) \\ - \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7) - 211(14) 40(5) - 0.61(5) b.d.l	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ 44(2) \\ 41(2) \\ - \\ 1.22(12) \\ b.d.l. \\ - \end{array}$	N(P) = 6 4.13(15) 669(17) 85(11) 6333(535) 5212(490) 5664(365) 209(17) 108(8) 1.9(1) 12(1) 0.65(4) 57(4) - 58(2) 43(3) - b.d.l.	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55) 311(20) 0.11(1) 1.40(48)	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) - 1470(437) 1012(226) b.d.l. 33(8)	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \\ - \\ 934(36) \\ 21(4) \\ - \\ - \\ b.d.l. \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ $	$\begin{array}{c} N(P) = 8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ 301(15)\\ 13(1)\\ -\\ -\\ -\\ b.d.l.\\ -\\ -\end{array}$	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr Mo Cd In Sn Sb Te	N (P) = 10 4.74(11) 818(20) 77(4) 5372(218) 4782(209) 5013(128) 98(4) 45(2) 2.3(3) 14(1) 1.15(6) 30(1) - - 414(20) 19(1) - b.d.l. 0.13(1) - -	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7) 211(14) 40(5) - 0.61(5) b.d.l	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \\ - \\ 1.22(12) \\ b.d.l. \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ - \\ $	N(P) = 6 4.13(15) 669(17) 85(11) 6333(535) 5212(490) 5664(365) 209(17) 108(8) 1.9(1) 12(1) 0.65(4) 57(4) - - 58(2) 43(3) - - b.d.l. -	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55) 311(20) 0.11(1) 1.40(48) 303(27)	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) - 1470(437) 1012(226) b.d.l. 33(8) 1549(310)	N(P) = 7 12.88(59) 2080(84) 226(20) 14875(652) 12230(570) 16696(549) 71(3) 12(1) 2.0(2) 37(2) 1.7(1) 3.8(4) - - 934(36) 21(4) - b.d.l. -	$\begin{array}{c} N(P) = 8\\ 5.24(30)\\ 864(36)\\ 126(6)\\ 7126(321)\\ 5853(259)\\ 8594(222)\\ 94(5)\\ 33(2)\\ 0.80(12)\\ 14.4(4)\\ 19(1)\\ -\\ -\\ -\\ 301(15)\\ 13(1)\\ -\\ -\\ -\\ b.d.l.\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\ -\\$	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8) 1246(49) - 5158(238) 941(52) 0.16(3) 0.52(9) 40(4)
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ge As Se Zr Mo Cd In Sn Sb Te W	$\begin{array}{c} N\left(P\right) = 10 \\ 4.74(11) \\ 818(20) \\ 77(4) \\ 5372(218) \\ 4782(209) \\ 5013(128) \\ 98(4) \\ 45(2) \\ 2.3(3) \\ 14(1) \\ 1.15(6) \\ 30(1) \\ - \\ - \\ 414(20) \\ 19(1) \\ - \\ - \\ b.d.l. \\ 0.13(1) \\ - \\ - \\ 116(3) \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7) 211(14) 40(5) - 0.61(5) b.d.l 145(13)	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \\ - \\ 1.22(12) \\ b.d.l. \\ - \\ 310(24) \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ 192(10) \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55) 311(20) 0.11(1) 1.40(48) 303(27) -	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) - 1470(437) 1012(226) b.d.l. 33(8) 1549(310) -	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \\ - \\ 934(36) \\ 21(4) \\ - \\ - \\ b.d.l. \\ - \\ - \\ 238(22) \end{array}$	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5) 33(2) 0.80(12) 14.4(4) 19(1) 301(15) 13(1) b.d.l 181(24)	
CaO (wt.%) Ti (ppm) P V Cr Mn Co Ni Cu Zn Ga Ga Ga As Se Zr Mo Cd In Sh Te W Ph	$\begin{array}{c} N\left(P\right) = 10 \\ 4.74(11) \\ 818(20) \\ 77(4) \\ 5372(218) \\ 4782(209) \\ 5013(128) \\ 98(4) \\ 45(2) \\ 2.3(3) \\ 14(1) \\ 1.15(6) \\ 30(1) \\ - \\ - \\ 414(20) \\ 19(1) \\ - \\ b.d.l. \\ 0.13(1) \\ - \\ - \\ 116(3) \\ b.d.l \\ \end{array}$	N(P) = 7 2.60(18) 442(21) 60(5) 4660(644) 3875(668) 5259(971) 159(19) 83(10) 1.27(17) 9.6(17) 0.44(4) 50(7) 211(14) 40(5) - 0.61(5) b.d.l 145(13) 0.32(7)	$\begin{array}{c} N(P) = 7 \\ 4.91(15) \\ 823(27) \\ 102(6) \\ 5243(225) \\ 4712(219) \\ 5011(108) \\ 150(6) \\ 71(4) \\ 1.8(1) \\ 17(1) \\ 0.67(5) \\ 36(2) \\ - \\ - \\ 44(2) \\ 41(2) \\ - \\ 1.22(12) \\ b.d.l. \\ - \\ 310(24) \\ 0.21(2) \end{array}$	$\begin{array}{c} N(P) = 6 \\ 4.13(15) \\ 669(17) \\ 85(11) \\ 6333(535) \\ 5212(490) \\ 5664(365) \\ 209(17) \\ 108(8) \\ 1.9(1) \\ 12(1) \\ 0.65(4) \\ 57(4) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ 58(2) \\ 43(3) \\ - \\ - \\ 192(10) \\ 0.26(3) \end{array}$	- 4.99(22) 825(28) - - 972(98) 853(32) - 46(5) 2.1(3) 11(1) 0.77(3) - b.d.l. 1121(105) 141(8) - 782(55) 311(20) 0.11(1) 1.40(48) 303(27) - 248(44)	- 3.11(34) 504(54) - - 690(18) 506(46) - 250(78) 6.1(12) 11(1) 0.77(11) - 7.1(24) 2436(354) 84(13) - 1470(437) 1012(226) b.d.l. 33(8) 1549(310) - 611(207)	$\begin{array}{c} N(P) = 7 \\ 12.88(59) \\ 2080(84) \\ 226(20) \\ 14875(652) \\ 12230(570) \\ 16696(549) \\ 71(3) \\ 12(1) \\ 2.0(2) \\ 37(2) \\ 1.7(1) \\ 3.8(4) \\ - \\ - \\ 934(36) \\ 21(4) \\ - \\ - \\ b.d.l. \\ - \\ - \\ 238(22) \\ 0.77(4) \end{array}$	N(P) = 8 5.24(30) 864(36) 126(6) 7126(321) 5853(259) 8594(222) 94(5) 33(2) 0.80(12) 14.4(4) 19(1) 301(15) 13(1) - b.d.l 181(24) 0 16(2)	- 11.95(18) 1959(50) - - 3339(63) 1858(31) - 28(1) 1.18(10) 33(1) 1.6(1) - b.d.l. 234(8) 1246(49) - 5158(238) 941(52) 0.16(3) 0.52(9) 40(4) - 1534(61)

^a Number of analyses ^b Number in brackets represent 2 SE in terms of least digits cited ^c b.d.l. = below detection limit ^d n.d. = not determined

Run #	PR1446	PR1449	PR1450	PR1465	PR1468	PR1470	PR1477	PR1480	PR1481	PR1489	PR1491	PR1505	PR1506	PR1508
EPMA (wt.%)	N = 30 ª	N = 29	N = 6	N = 45	N = 29	N = 30	N = 30	N = 12	N = 8	N = 25	N = 34	N = 27	N=26	N = 12
	00 40(40)h	05 57(40)	00.00/457)	00.05(54)	05 77(40)	00.00(00)	0.4.00(0.4)	07.00(00)	00.00/05)	00 54(400)	05 50(404)	00.00(05)	04.00(00)	00.04(4.40)
re Ni	86.12(12)	85.57(46)	82.98(157)	80.05(51)	85.77(42)	90.32(86)	84.92(64)	87.92(80)	92.00(35)	88.54(168)	85.56(101)	89.99(35)	91.60(33)	82.64(140)
	5.13(4)	4.03(5)	5.21(21)	5.40(4)	4.69(6)	1.20(3)	5.09(6)	4.35(8)	0.07(2)	5.15(13)	5.63(11)	1.29(1)	1.47(1)	5.30(15)
Cr Ma	D.d.I.	0.09(2)	0.08(3)	0.030(4)	0.039(8)	0.31(1)	0.07(1)	0.06(1)	0.28(2)	0.12(5)	0.07(3)	0.35(1)	0.16(1)	0.16(4)
	-	-	-	-	-	1.73(20)	-	-	0.30(4)	-	-	1.00(13)	1.46(10)	-
VV D	-	-	-	-	-	1.29(5)	-	-	1.73(12)	-	-	1.43(4)	1.34(4)	-
F C-	-	-	-	-	-	1.31(44)	-	-	0.56(10)	-	-	1.10(14)	0.47(7)	-
	-	-	-	-	-	1.02(1)	-	-	1.10(3)	-	-	1.00(1)	1.70(1)	-
Ge	- 6 d l 6	-	- b d l	-	-	1.44(5)	-	- b d l	0.45(4)	- b d l	-	1.04(4)	1.43(2)	-
win V	D.Q.I.*	0.007(3)	D.U.I.	0.006(2)	0.004(2)	0.014(4)	0.006(3)	D.U.I.	0.03(1)	D.U.I.	0.004(2)	0.038(5)	0.01(1)	0.03(2)
v In	-	- 1 25(11)	-	-	- 0.82(10)	0.036(4)	- 1 40(17)	- 1 16(19)	0.05(1)	– ndd	- 1 51(10)	0.054(5)	0.014(5)	- 1 46(17)
[]]	0.51(1)	1.23(11)	0.00(20)	1.11(10)	0.02(10)	-	1.49(17)	1.10(10)	-	0.07(7)	1.51(19)	-	-	1.40(17)
Cu Sh	0.023(3)	0.09(9)	0.33(13) 2 14(61)	1 94(15)	0.09(2)	-	0.03(9)	0.19(3)	-	0.07(7)	0.04(20)	-	-	0.00(7)
SD Dh	0.05(1)	2.00(12)	2.14(01)	0.47(5)	3.22(13)	-	2.27(13)	1.07(20)	-	0.22(15)	2.03(22)	-	-	2.40(23)
FU So	0.03(1)	1.09(12)	0.42(14) 1 24(45)	0.17(3) 0.57(14)	0.00(3)	-	1.03(12)	0.10(4) 0.70(13)	-	0.23(13)	0.09(40)	-	-	0.30(0) 1.27(24)
	0.00(1)	0.80(8)	0.65(17)	0.37(14)	0.30(13)	-	1.74(23)	0.70(13)	-	0.00(02) n.d	0.09(10)	-	-	1.27(24)
Λe	0.04(1)	0.00(0)	0.03(17) 1 $45(21)$	0.21(3) 1 11(0)	0.33(0)	-	1 42(6)	0.32(0) 1 42(11)	-	1.u. 1.62(22)	1.52(9)	-	-	0.56(11)
AS Total	2.40(4)	1.29(3)	05 37(50)	07 25(15)	07.08(25)	-	1.42(0)	08 17(25)	-	06 62(75)	09 61(29)	-	-	05 80(122)
Total	97.55(9)	90.72(19)	95.57(50)	97.33(13)	97.90(23)	99.41(13)	99.19(13)	90.17(33)	97.54(19)	90.02(75)	90.01(20)	99.42(12)	99.75(21)	95.00(125)
LA-ICP-MS	n.a. ^d	N = 9	N = 15	N = 13	N = 5	N = 12	N = 8	N = 9	n.a.	N = 12	N = 9	N = 9	N = 11	N = 12
	_	-	-	-	-	N(P) = 3	-		_		-	N(P) = 5	N(P) = 7	-
D						10010(1005)						12040(962)	6102(646)	
r n e	-	-	-	-	-	10916(1295)	-	-	-	-	-	13949(003)	0193(040) 5079(520)	-
Pcorr ⁻	-	-	-	-	-	0903(100Z)	-	-	-	-	-	11430(700)	2078(230) 124(67)	-
v	-	-	-	-	-	192(21)	-	-	-	-	-	404(23)	134(07)	-
V corr Cr	-	-	- 711(97)	- 315(35)	– hdl	209(29)	-	- 200(78)	-	- 774(122)	-	2042(66)	100(94)	-
Ur Mn	-	1200(09)	111(07)	313(33)	b.u.i.	2020(74)	509(04)	290(70)	-	67(15)	370(90)	3042(00)	240(20)	1003(41)
Co	-	114(20)	124(20)	24(4)	D.U.I.	343(29) 12712(205)	50(9)	00(17)	-	07(15)	40(0)	441(30)	240(39)	272(33)
Ni	-	_ Int ^f	_ Int	_ Int	_ Int	127 12(203)	_ Int	_ Int	-	_ Int	_ Int	127 13(09) Int	15203(309) Int	_ Int
	_	71(2)	78(6)	78(4)	56(9)	60(3)	81(5)	86(9)	_	75(8)	82(3)	36(6)	34(2)	81(8)
Cu	_	7 T(2) 46(1)	51(4)	51(3)	36(6)	30(2)	52(3)	56(6)	-	19(5)	54(2)	23(4)	22(1)	53(5)
Zucorr Zn	_	73(5)	85(0)	62(6)	165(85)	15/(12)	$\frac{32(3)}{142(15)}$	180(24)	2	112(18)	$\frac{34(2)}{92(10)}$	$\frac{23(4)}{74(7)}$	63(10)	137(14)
Zn	_	18(1)	20(2)	15(1)	40(20)	37(3)	34(4)	43(6)	_	27(4)	22(2)	18(2)	15(2)	33(3)
Ga	_	27(2)	22(2)	3 0(2)	~9.4	3 8(6)	4 8(6)	5 8(12)	_	24(5)	29(2)	3 3(4)	2 4(4)	2 3(3)
Ga		2.1(2)	1 7(2)	2.3(1)	<7.2	3.0(5)	3 7(5)	4 5(10)	_	1 9(4)	2.3(2) 2.2(1)	2 6(4)	1 9(3)	1.8(3)
Ge	_	_	_	-	_	12597(332)	-	-	_	-	_	16489(333)	14692(209)	-
As	_	13230(253)	14432(442)	13608(637)	13097(2083)	51(6)	14846(349)	16327(497)	_	17206(1289)	17243(433)	-	-	15452(547)
Se	_	17769(1388)	21356(2920)	10099(1350)	15183(3200)	-	23092(1845)	16561(2316)	_	21523(4064)	8121(1273)	_	_	17486(2585)
Secore	_	12794(999)	15376(2102)	7271(972)	10932(2304)	_	16626(1328)	11924(1668)	_	15497(2926)	5847(917)	_	_	12590(1861)
Mo	_	_	_	_	_	10395(579)	_	_	_	_	_	13008(640)	10618(684)	_
Mocorr	_	_	_	_	_	16424(915)	_	_	_	_	_	20553(1011)	16776(1081)	_
Cd	_	25976(3005)	43765(7114)	9424(1424)	11365(4681)	_	34171(5238)	39603(8860)	_	50440(14501)	12432(2267)	_	_	39404(13612)
Cdcorr	_	3637(421)	6127(996)	1319(199)	1591(655)	_	4784(733)	5544(1240)	_	7062(2030)	1740(317)	_	_	5517(1906)
In	_	20862(1952)	22917(3165)	24177(2871)	21530(4466)	<40	31838(2823)	38502(5140)	_	25128(3858)	23543(3193)	<17	bdl	30525(4110)
Incorr	_	10222(956)	11229(1551)	11847(1407)	10550(2188)	<2.0	15601(1383)	18866(2519)	_	12313(1890)	11536(1565)	<0.8	_	14957(2014)
Sn	_	18(1)	8.5(8)	7.3(5)	17(6)	7.2(12)	11(1)	16(2)	_	4.6(9)	5.8(5)	5.0(7)	4.4(7)	5.2(8)
Sncorr	_	13(1)	6.2(6)	5.4(4)	12(4)	5.3(9)	7.7(7)	11(2)	_	3.3(7)	4.3(4)	3.7(5)	3.2(5)	3.8(6)
Sb	_	23807(974)	23724(1859)	24868(1358)	29610(5986)	_	27637(1297)	24801(1264)	_	32642(3354)	33238(1197)	_	_	30724(1501)
Sbcorr	_	17617(721)	17556(1376)	18402(1005)	21911(4430)	_	20451(960)	18353(935)	_	24155(2482)	24595(886)	_	_	22736(1111)
Te	_	16413(1660)	24783(4312)	7093(985)	15621(4309)	_	27452(2769)	25082(5308)	_	25345(5433)	10141(1621)	_	_	28689(6495)
Tecorr	_	6401(647)	9665(1682)	2766(384)	6092(1681)	_	10706(1080)	9782(2070)	_	9885(2119)	3955(632)	_	_	11189(2533)
W	_	_	_	_	_	7717(606)	_	_	_	_	-	9374(397)	7768(447)	_
Wcorr	_	_	_	_	_	13659(1073)	_	_	_	_	_	16592(703)	13749(791)	_

Table S.2 Chemical compositions of metal phases determined by EPMA and LA-ICP-MS.

Pb Pb _{corr}	- -	19735(2992) 7104(1077)	19532(3407) 7032(1227)	6337(894) 2281(322)	6137(2123) 2209(764)	15(2) 5.5(7)	22135(3101) 7968(1116)	21076(6781) 7587(2441)	-	21352(6103) 7687(2197)	9232(2050) 3323(738)	14(1) 5.0(4)	5.3(11) 1.9(4)	19408(6448) 6987(2321)
Run # EPMA (wt.%)	PR1510 <i>N</i> = <i>29</i>	PR1517 N = 29	PR1518 N = 32	PR1521 N = 28	PR1522 <i>N</i> = 30	PR1524 N = 21	PR1538 N = 29	PR1539 N = 26	PR1561 <i>N</i> = 30	_				
Fe Ni Cr Mo W P Co Ge Mn V In Cd Sb Pb Se Te As Total	87.89(10) 0.79(1) 1.03(1) 1.27(4) 1.44(3) 0.11(1) 1.11(1) 0.38(2) 0.16(1) 0.29(1) - - - - - 94.48(9)	89.18(28) 1.47(1) 0.82(1) 1.90(11) 1.64(4) 0.81(9) 1.76(1) 1.47(3) 0.14(1) 0.25(1) - - - - - 99.48(14)	91.08(18) 1.43(1) 0.35(1) 1.44(7) 1.42(3) 0.78(7) 1.67(1) 1.39(2) 0.038(4) 0.030(5) - - - - - - 99.68(10)	89.66(22) 1.45(1) 0.79(1) 1.63(7) 1.58(4) 0.69(7) 1.75(1) 1.67(2) 0.11(1) 0.18(1) - - - - - 99.56(11)	88.20(56) 5.25(4) 0.04(1) - - - 0.005(3) - 1.11(15) 0.37(9) 2.00(13) 0.34(5) 0.99(17) 0.58(8) 1.40(5) 100.30(11)	82.38(136) 6.08(11) 0.04(1) - - - 0.004(3) - 1.59(31) 0.27(8) 3.34(44) 0.43(12) 0.61(17) 0.46(10) 2.04(11) 97.25(57)	91.75(13) 1.39(2) 0.18(2) 1.44(6) 1.51(3) 0.50(5) 1.71(2) 1.27(2) 0.016(5) 0.029(5) - - - - - - 99.82(11)	91.19(22) 1.40(1) 0.37(1) 1.65(11) 1.52(4) 0.73(7) 1.70(1) 1.36(2) 0.04(5) 0.046(5) - - - - - - 100.03(10)	84.51(67) 5.04(5) 0.07(1) - - - 0.004(2) - 1.47(14) 0.63(11) 2.01(15) 0.92(12) 1.94(23) 1.24(13) 1.24(13) 1.40(3) 99.26(13)					
LA-ICP-MS	N = 10 N (P) = 5	N = 11 N (P) = 5	N = 13 N (P) = 6	N = 12 N (P) = 4	N = 11	N = 11	N = 8 N (P) = 5	N = 9 N (P) = 6	N = 12	_				
P Pcorr V Vcorr Cr Mn Co Cu Cu _{corr} Zn Zn _{corr} Ga Gacorr Ge As Se Secorr Mo Mo _{corr} Cd Cd _{corr} Sh Sh _{corr} Sh	1562(117) 1281(96) 1685(56) 2359(78) 7516(168) 1512(102) 8759(59) Int. 35(3) 23(2) 50(11) 13(3) <2.4 <1.8 42251(33) - - 4220(350) 6668(553) - 0.23(6) 1.94(4) 1.42(29) - - 2952(437)	10455(575) 8573(472) 2047(107) 2866(150) 6882(128) 1372(38) 14623(85) <i>Int.</i> 29(1) 19(1) 93(4) 22(1) 2.0(3) 15182(195) - - 13336(379) 21071(599) - 16(1) 7.6(5) 4.8(4) 3.5(3) - - 10498(359)	9540(576) 7823(472) 363(62) 508(87) 3287(136) 571(105) 14015(106) <i>Int.</i> 32(1) 21(1) 98(9) 24(2) 4.1(3) 3.2(2) 14009(187) - - 12020(422) 18992(667) - - 14(1) 6.9(5) 7.2(9) 5.3(7) - - - - 9553(275)	11572(950) 9488(779) 1763(110) 2468(154) 7411(214) 1436(99) 14117(146) <i>Int.</i> 29(5) 19(3) 148(20) 35(5) <4.4 <3.4 15672(196) - - 10151(1338) 16039(2114) - b.d.l. - 6.6(13) 4.8(9) - - - 6667(1073)	- - - 528(87) 60(8) - Int. 67(5) 44(3) 125(14) 30(3) 3.5(2) 2.7(2) - 15346(484) 13206(1871) 9508(1347) - 21461(6954) 3004(974) 20019(3469) 9809(1700) 6.8(4) 5.0(3) 26073(1356) 19294(1003) 16828(5644) 6563(2201) -	- - 440(85) 44(11) - Int. 89(4) 58(3) 161(11) 39(3) 3.6(4) 2.8(3) - 21271(740) 12077(976) 8695(703) - 21584(2712) 3022(380) 38271(3828) 18753(1876) 9.6(10) 7.0(7) 45917(1558) 33979(1153) 15878(2017) 6192(787) -	6785(634) 5564(520) 456(77) 638(108) 2156(205) 308(47) 13931(192) <i>Int.</i> 19(1) 12(1) 53(4) 13(1) -3.4 -2.7 12974(412) - - 7495(937) 11842(1480) - - 3.8(8) 2.8(6) - - - 6272(656)	9352(956) 7669(784) 392(77) 549(108) 3540(199) 563(62) 13777(166) <i>Int.</i> 28(4) 18(3) 144(17) 35(4) b.d.l. - 13796(437) - - 11845(1170) 18720(1849) - b.d.l. - <10 <7.3 - - 8151(408)	- - 784(48) 35(5) - Int. 83(4) 54(3) 69(4) 17(1) 3.2(3) 2.5(3) - 14800(296) 23399(1554) 16847(1119) - 3.2269(4170) 4518(584) 27271(2248) 13363(1102) 7.4(4) 5.4(3) 25315(713) 18733(528) 30756(3035) 11995(1184) -					

W _{corr}	5225(774)	18582(635)	16909(469)	11801(1899)	-	-	11101(1161)	14427(722)	-
Pb	2.4(2)	14(1)	8.9(14)	16(2)	15182(7155)	14518(2700)	5.9(10)	12(1)	22925(3563)
Pb _{corr}	0.86(7)	5.0(4)	3.2(5)	5.9(7)	5465(2576)	5227(972)	2.1(4)	4.5(3)	8253(1283)

^a Number of analyses ^b Number in brackets represent 2 SE in terms of least digits cited ^c b.d.l. = below detection limit ^d n.a. = not analysed; n.d. = not determined ^e Calculated using correction factors listed in Table S1 ^f Used as internal standard for LA-ICP-MS data processing

	Potential contribution (in %) to bulk	Potential contribution (in %) to bulk
	silicate Moon abundances	silicate Moon abundances
	by delivery of CI chondrites	by delivery of H chondrites
Cu	0.4–0.9	0.2–0.6
Zn	0.8–2.0	0.1–0.3
Ga	0.08–0.21	0.05–0.13
Ge	43–107	17–42
Se	17–42	6–16
Cd	1–3	0.02–0.05
In	1–2	0.2–0.5
Sn	1–2	0.4–1.1
Те	11–28	3–6
Pb	2–4	0.17–0.43

Table S.3 Calculated maximum contribution (in %) of a CI- or H chondritic 0.02-0.05 mass% late veneer to the estimated lunar mantle abundances of volatile siderophileand chalcophile elements