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Evaporation of moderately volatile elements from metal and sulfide melts: Implications for volatile element abundances in magmatic iron meteorites

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ARTICLE INFO

Article history: Received 22 February 2023 Received in revised form 13 September 2023 Accepted 14 September 2023 Available online xxxx Editor: F. Movnier Keywords: iron meteorite moderately volatile elements accretion experimental petrology evaporation

ABSTRACT

Volatile element abundances in magmatic iron meteorites provide fundamental insights into the processing of volatile elements in the early solar system. Although Cu, Ge and Ag concentrations of magmatic iron meteorites deviate up to 4 orders of magnitude between different magmatic iron meteorite groups, the role of evaporation on these volatile abundances is poorly constrained. Here, we experimentally assess the volatility of Cu, Ge, Ag, S, Cr, Co, Ni, Mo, Ru, Pd, W, Re and Ir from metal and sulfide melts as a function of pressure $(10^{-4} \text{ and } 1 \text{ bar})$, temperature (1573-1823 K) and time (5-120 min) for two end-member compositions (Fe versus FeS). These novel experiments demonstrate that the presence of S is a major parameter in establishing the volatility of Cu, Ge, Mo, Ag, Ru, W, Re and Ir. At constant P-T and time, the volatility of Ge, Mo, Ru, W, Re and Ir is greatly increased in the presence of S, whereas Cu and Ag are less volatile in the presence of S. At 1773 K and \sim 0.001 bar, the volatility of S is sufficiently high that the degassed FeS liquid showed immiscibility of a Srich sulfide and a S-poor Fe melt. Empirical equations were derived that predict the evaporative loss of Cu, Ge, Mo, Ag from Fe and/or FeS liquid as a function of temperature and time. A comparison of the newly derived volatility sequences with commonly applied 50% condensation temperature models shows that the condensation temperature models cannot be applied to sulfur-bearing Fe liquids and therefore to magmatic iron meteorites. Application of the new models on previously derived elemental depletions in the IVB parent body shows that evaporation, if it occurred, cannot have taken place under S-rich conditions. The latter would result in a depletion of Mo, which is not observed for the IVB irons. However, evaporation of a S-free or S-poor Fe liquid reproduces the observed volatility depletion trend for IVB irons under a wider range of temperature and evaporation times, demonstrating the potential importance of evaporative loss on the IVB parent body.

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1. Introduction

The chemical composition of magmatic iron meteorites provides fundamental insights into planetary accretion processes, such as the architecture of the early solar system (carbonaceous (CC) versus noncarbonaceous (NC) magmatic iron meteorites; Rubin, 2018), core crystallization (Campbell and Humayun, 2005; Chabot and Zhang, 2021) and devolatilization processes (Kleine et al., 2018; Gargano and Sharp, 2019; Hirschmann et al., 2021). Magmatic iron meteorites are primarily distinguished based on their trace element compositions and potentially represent the cores of more than 50 parent bodies (Goldstein et al., 2009). The primary dif-

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https://doi.org/10.1016/j.epsl.2023.118406

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ference between the different groups is the degree of depletion in volatile elements, which increases from type I to IV iron meteorites (Scott and Wasson, 1975). The class of the IVB iron meteorites is thus one of the most volatile element-depleted meteorite suites. As nucleosynthetic isotope anomalies of IVB iron meteorites revealed that these meteorites are indeed members of the carbonaceous chondrite group (Budde et al., 2016), they must have accreted beyond the ice line and therefore may have been very rich in volatile and moderately volatile elements initially (Kruijer et al., 2017). However, similar bulk Ga and Ge concentrations of CC and NC magmatic iron meteorites do not suggest significantly different initial volatile contents of bulk CC and NC parent bodies The exact processes (i.e., nebular versus at the time of accretion) responsible for the volatile loss in magmatic irons, including IVB's, therefore remain uncertain. Depletions could have been in-

Please cite this article as: E.S. Steenstra, C.J. Renggli, J. Berndt et al., Evaporation of moderately volatile elements from metal and sulfide melts: Implications for volatile element abundances in magmatic iron meteorites, Earth and Planetary Science Letters, https://doi.org/10.1016/j.epsl.2023.118406

(Rubin, 2018).

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1 herited from incorporation of chondritic precursor material (Sears, 2 1978; Wai and Wasson, 1979; Scott, 1979; Chen et al., 2013) 3 and/or result from volatile loss during large impact events (Horan et al., 2012). Campbell and Humayun (2005) proposed that nebu-4 5 lar processing controlled their abundances, based on the relative 6 abundances of refractory siderophile elements in the IVB parent 7 melt. On the other hand, Fe, Cr and W (but not Ni or Co) have been 8 inferred to have been lost at $\sim \Delta IW = -1$ prior to fractional crysq tallization of the IVB melt (Rasmussen et al., 1984; Campbell and 10 Humayun, 2005). Campbell and Humayun (2005) observed that 11 elements with a condensation temperature below Fe are increas-12 ingly depleted in the IVB meteorites. Davis (2006) also concluded 13 that Ge/Ni varies strongly for different magmatic iron meteorite 14 classes, but with very limited intra-group variation. Given that 15 Ge/Ni is hardly affected by core crystallization processes and Ni is 16 non-volatile, Ge must have been lost due to volatility-related frac-17 tionation. Kleine et al. (2018) reported new Ag isotopic data for 18 IVB's that would be most consistent with loss of volatiles from a 19 molten metallic core while exposed to space, after a catastrophic 20 disruption of the parent body. Such volatile loss would also be con-21 sistent with previous models that suggested that the IVB parent 22 body may have experienced internal temperatures exceeding 1760 23 K (Campbell and Humayun, 2005). It has been proposed that the 24 IVA parent body core may also have experienced evaporative loss 25 of Ag (Horan et al., 2012) due to impact disruption and removal 26 of the mantle. Such an event is also suggested from the inverse 27 correlation of metallographic cooling rates and Ni contents or de-28 grees of fractional crystallization (Yang et al., 2007). Finally, it was 29 concluded that evaporation of Ag from metallic melts is a viable 30 model to account for Pd-Ag systematics of both the IVA (Matthes 31 et al., 2018) and IVB cores (Kleine et al., 2018).

32 Copper is the most depleted element in the IVB suite, although 33 Cu and d⁶⁵Cu are not correlated (Bishop et al., 2012). Copper iso-34 tope data for most magmatic iron groups, including IVB's, also have 35 strongly negative δ^{65} Cu values (i.e., down to -2.26%), the opposite of what would be expected if Cu was predominantly lost 36 through evaporation (Bishop et al., 2012; Chen et al., 2016). How-37 38 ever, Chen et al. (2016) showed that the δ^{65} Cu data for the IVB 39 suite are strongly modified by neutron capture, through the reac-40 tion ${}^{62}Ni(n,\gamma){}^{63}Ni$ followed by beta decay to ${}^{63}Cu$, and proposed an average pre-exposure value of δ^{65} Cu of $-0.3\pm0.8\%$, within 41 42 the range of other iron meteorite groups and chondrites. Alto-43 gether, this could suggest that Cu was not lost due to volatility-44 related fractionation. This highlights the difficulties to ascribe 45 mass-dependent processes unambiguously as Cu only has 2 isotopes, in conjunction with the aforementioned significant nucle-46 47 osynthetic variations among chondrites (Luck et al., 2003, 2005). 48 Finally, it could reflect initial extensive evaporation, followed by 49 partial recondensation of Cu in the kinetic regime, as proposed for 50 K in angrites (Hu et al., 2022). Tungsten and Cr may have been lost 51 early (Rasmussen et al., 1984; Campbell and Humayun, 2005), con-52 sistent with the observed anomalous behavior of W compared to 53 Mo in magmatic iron meteorites, as they are expected to exhibit 54 similar geochemical behavior (Scott, 1978).

55 Volatile loss may have been significant for S, as it is commonly assumed to be more volatile than Cu, at least during condensa-56 tion from a highly reduced solar gas at 10^{-4} bar (e.g., Wood et 57 58 al., 2019). Previous studies showed that iron meteorites typically 59 contain bulk S contents of approximately 0 to 2 wt.% (Buchwald, 1975). However, it is believed that many magmatic iron meteorite 60 61 parent bodies were potentially far richer in S (up to 10% bulk core 62 S; Chabot and Zhang, 2021) and that samples of S-rich portions 63 were perhaps selectively destroyed (Hirschmann et al., 2021 and 64 references therein). Depending of the difference in volatility of el-65 ements for S-bearing and S-free metal alloys, depletions of such 66 elements may be used to investigate the timing of S loss from magmatic iron meteorites. To investigate the nature of volatile el-
ement depletions in magmatic iron meteorites, novel degassing
experiments were conducted to systematically quantify the (po-
tential) evaporative loss of Cr, Cu, Ge, Ag and W from metal and
sulfide melts. Several other, nominally non-volatile elements (Co,
Ni, Mo, Ru, Pd, Re and Ir) were added to assess their volatility in
S-free and S-rich metal melts.67
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2. Methods

2.1. Experimental

Metal and sulfide mixtures were melted in a gas mixing furnace at the Institute of Mineralogy, University of Münster. Experiments were conducted at both 1 bar and at low vacuum (\sim 0.0007–0.0013 bar) for variable run times (5-120 min). Peak temperatures of 1573-1823 K were explored and correspond with peak thermal conditions typically inferred for asteroidal differentiation processes (e.g., Campbell and Humayun, 2005). Experiments run at 1 bar were flushed with pure CO and buffered the experiments with the graphite buckets at the graphite - CO (GCO) buffer. Temperatures were monitored and controlled using a type B thermocouple and a Eurotherm 3508 programmable controller. The estimated temperature uncertainties are less than 5 degrees. Vacuum was attained in the furnace by attaching an Alcatel vacuum pump to the lower end of the vertical furnace tube (alumina) and sealing the gas-input valve at the top of the furnace. The pressure was monitored with an Edwards vacuum gauge controller. The vacuum experiments were conducted by first ramping the furnace up to the target temperature, without any sample present. The sample hanger and sample were then hung in the top section of the furnace, far away from the hotspot, and the furnace was subsequently depressurized. When the target pressure was reached, the sample holder and sample were rapidly lowered into the hot spot.

Starting compositions consisted of high-purity FeS or Fe pow-101 ders doped with 0.1 mol% of high-purity Cr, Co, Ni, Cu, Ge, Mo, 102 Ru, Pd, Ag, W, Re and Ir powders. Two end-member starting com-103 positions (Fe + traces, FeS + traces) were chosen to explore the 104 effects of S on the volatility of the elements of interest. Mixtures 105 were mixed in an agate mortar under ethanol for at least 30 min to 106 ensure homogeneous starting compositions. Trace-element doped 107 sulfide and metal powders were loaded in separate, ~ 2 cm long 108 graphite buckets (\sim 4–5 mm O.D., \sim 3 mm I.D.) that in turn were 109 placed in a larger single graphite bucket of \sim 4–5 cm long and 2–3 110 cm wide. The graphite buckets were suspended by Pt or Re wire 111 depending of the experimental conditions. The graphite capsules 112 were filled to approximately 2/3 of their length by using pins to 113 ensure proper packing of the starting mixtures. Although the use 114 of graphite buckets inevitably results in the presence of C in Fe 115 and to a lesser extent FeS liquid, graphite was found to be the 116 most convenient bucket material due to its high melting point, 117 limited weight and softness allowing for simple machining. Runs 118 performed with FeS powders under vacuum were initially chal-119 120 lenging due to the consistent loss of the FeS powder charge from the graphite capsule at the onset of depressurizing, despite careful 121 and tight packing of the powder in the capsule. Post-experimental 122 123 investigation showed that these mixtures were only sintered and 124 not quenched, suggesting run products were rapidly lost from the hotspot in the first few seconds of the experiment. This issue was 125 addressed by drilling a small hole (0.5-1.5 mm diameter) in the 126 127 bottom of the graphite capsule in conjunction with pressing of the FeS powder into a dense pellet at room temperature. Using this 128 approach, such vacuum-driven losses were subsequently largely 129 prevented. However, preferably a solid starting material is used 130 rather than a powder. This is because there are potential time lag 131 effects associated with the melting of a powder (Sossi et al., 2019), 132

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relative to the use of a solid material, potentially yielding an over-

2 estimation of the time during which a melt can effectively degas. 3 However, the melting of the starting materials of interest would inevitably result in large elemental losses due to its very low viscosity in conjunction with the expected volatility of the elements 6 of interest. Therefore, powdered starting materials were used for all experiments.

After the experiments, the retrieved run products were mounted in epoxy resin and polished using various grades of SiC sandpaper and polycrystalline diamond spray. The samples were carboncoated for imaging and chemical analyses of major elements by electron microprobe, after which they were analyzed for trace elements by LA-ICP-MS.

2.2. Analytical

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In all of the analyses, except for ¹⁰¹Ru and ¹⁹³Ir, the NIST 67 610 glass was used as an external reference material for both 68 high-pressure synthesized starting materials and experimental 69 run products (Jochum et al., 2005a). The use of the non-matrix-70 matched NIST 610 glass for quantification of absolute elemental 71 concentrations in FeS- and Fe-based samples will certainly yield 72 significant matrix effects, particularly for nominally volatile and 73 refractory elements such as Ge, Ir, W, Re (Steenstra et al., 2019, 74 2020; Fig. S.3). The high-pressure synthesized metals and sulfides 75 76 have a (near)-identical composition to the degassed samples in terms of major elements (Fe, S). Given that the reported evapora-77 78 tive loss factors are defined simply as ratios relative to the high P-T starting material, any matrix effects arising from the use of 79 non-matrix matched reference materials would thus be effectively 80 canceled out. For quantification of ¹⁰¹Ru and ¹⁹³Ir abundances, a 81 Cu and/or Ni sulfide (Wohlgemuth-Ueberwasser et al., 2007) and 82 the GSD-1G glass (Jochum et al., 2005b) was used, respectively. The 83 Fe abundances (assuming ⁵⁶Fe) of metals and sulfides as measured 84 by electron microprobe were used as internal standards in all anal-85 yses. The LA-ICP-MS data was reduced using GLITTER software (van 86 Achterbergh et al., 2001; Griffin et al., 2008) and included moni-87 toring and/or identification of heterogeneities or potential spatial 88 compositional variations in the exposed section through the run 89 90 products. 91

3. Results

3.1. Run products

Run products were generally characterized by a single quenched metal or sulfide blob embedded within the graphite bucket (Fig. 1). Although texture types varied greatly between run products obtained at different temperatures (Fig. 1), all samples showed textures indicative of metals and sulfides being fully molten at the time of quenching. This is consistent with phase diagrams that predict that C-saturated Fe liquid and FeS liquid are fully molten above ~ 1545 K and 1420 K at ambient pressures, respectively (Lord et al., 2009; Buono and Walker, 2011, and references therein). Quenched metal liquids show small graphite inclusions throughout the samples (Fig. 1a-c), in agreement with a C-saturated state of the metallic liquid. Carbon concentrations were not directly measured but can be roughly assessed for Fe liquid experiments by consideration of the EPMA totals (Table S.2).

Some of the sulfide liquids degassed under vacuum experienced 110 extensive loss of S, resulting in the immiscibility of a S-poor, C-rich 111 Fe liquid and a S-rich, C-poor FeS melt (Fig. 1e; Table 1), consis-112 tent with previously derived phase equilibria predictions (Corgne 113 et al., 2008). In the runs conducted over the longest run times 114 (120 min) at 1773 K almost all S degassed (Table 1). The FeS sam-115 ples also often contain tiny (<10 µm) Ru-, W-, Re- and/or Ir-rich 116 blebs, which contain almost the bulk inventory of the latter el-117 ements (see also next section). The formation of the latter blebs 118 is a direct result of their low solubility in FeS matte (Fonseca et 119 al., 2007, 2011). To obtain representative bulk compositions of the 120 samples that contained either immiscible C- and S-rich molten al-121 loy or PGE-rich nuggets, modal analyses were performed by using 122 the backscattered electron images of the experiments in conjunc-123 tion with image processing software Image Color Extract Tool®. 124 The bulk compositions of the samples were then calculated by us-125 ing the measured compositions of the different phases with the 126 derived modal abundances of the phases (Table S.2). Finally, some 127 disagreement is observed between the expected starting mix com-128 position and the measured starting composition synthesized at 129 high P-T (e.g., W). This is most likely the result of complex ma-130 trix effects arising from using the non-matrix-matched NIST-610 131 glass for the LA-ICP-MS analyses of metal and sulfide matrices 132

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Fig. 1. Backscattered electron images of typical experimental run products. Panels **a-c** depict run products for Fe melts, showing a variety of quench textures (**b**, **c**) with abundant graphite inclusions. Pits are LA-ICP-MS spots placed in horizontal and/or vertical transects. Panels **d-f** show run products using a FeS starting composition, with typical cracks formed during quenching and other quench textures. Panel *e* shows experiments CRESS-39, in which S degassing was sufficiently high to result in immiscibility of a S-poor, C-rich and S-rich, C-poor Fe liquid.

(e.g., Steenstra et al., 2019, 2020) and/or small uncertainties in the weighing of the starting mixtures. However, given that the experimental samples are normalized relative to the high *P*-*T* synthesized starting composition, matrix effects and/or weighing errors do not affect the presented results.

3.2. Homogeneity of quenched metal and sulfide liquids

Metal and/or sulfide liquids may be heterogeneous if degassing of the elements of interest is diffusion-limited within the liquid. To assess the potential of heterogeneous distribution of trace ele-ments in the experimental quenched liquids, LA-ICP-MS spots were placed in horizontal and/or vertical raster lines (Fig. 2). Only very limited variation of measured element contents between very dif-ferent areas of the samples is generally observed. This suggests that the very low viscosities of both the sulfide and metal melts are sufficient for maintaining a homogeneous distribution of trace elements throughout the melts despite evaporation. A notable exception is the large variation in Ru, W, Re, Ir abundances in sulfide melts, especially at lower temperatures, which is instead due to the presence of nuggets due to their oversaturation in FeS liquid as previously discussed. It should be noted that these nuggets are minor in abundance (<0.83 modal %) and do not contain significant amounts of Ni and other elements of interest, thereby not affecting the results for the other elements of interest (e.g., Cu, Ge, Mo, Ag).

Post-experimental results showed that some Fe liquid experiments that were conducted at 1 bar together with FeS melts – although at a distance and isolated in tall graphite buckets - suffered from some S cross-contamination (Fig. S.4). No other elemental cross-contamination was observed. An increase of S contents relative to starting compositions was only found to be significant for experiments CRESS-5 to 8 Fe, and CRESS-26 Fe, 27 Fe, 32 Fe and 38 Fe, with post-experimental S abundances of up to 0.76 wt.%, but usually much less (<0.30 wt.) (Table S.1).

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Table		Table	1
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Experimental run conditions.

3		Т	Р	Time	Starting comp ^a	Observed phases ^b	$\log f^{(S/Ni)}$	Comments	69
4		(K)	(bar)	(min)	5 T	r in r	- 05		70
5	CRESS-5 Fe	1673	1	15	Fe A	Fe	_	Performed together with CRESS-5 FeS	71
6	CRESS-5 FeS	1673	1	15	FeS A	FeS. Fe-W-Re-Ir allov	-0.06(5)	Performed together with CRESS-5 Fe	72
7	CRESS-6 Fe	1773	1	15	Fe A	Fe	_	Performed together with CRESS-6 FeS	73
,	CRESS-6 FeS	1773	1	15	FeS A	FeS, Fe-W-Re-Ir alloy	-0.02(3)	Performed together with CRESS-6 Fe	70
8	CRESS-7 Fe	1773	1	60	Fe A	Fe	-	Performed together with CRESS-7 FeS	74
9	CRESS-7 FeS	1773	1	60	FeS A	FeS, Fe-W-Re-Ir alloy	-0.04(3)	Performed together with CRESS-7 Fe	75
10	CRESS-8 Fe	1823	1	15	Fe A	Fe	-	Performed together with CRESS-8 FeS	76
11	CRESS-8 FeS	1823	1	15	FeS A	FeS, Fe-W-Re-Ir alloy	-0.05(5)	Performed together with CRESS-8 Fe	77
12	CRESS-10 Fe	1673	0.0004	15	Fe A	Fe	-	CRESS-10 FeS lost prior to melting ^c	78
10	CRESS-12 Fe	1773	0.0004	15	Fe A	Fe	-	CRESS-12 FeS lost prior to melting	70
13	CRESS-14 Fe	1573	0.0004	15	Fe A	Fe	-	CRESS-14 FeS lost prior to melting	79
14	CRESS-15 Fe	1623	0.0004	15	Fe A	Fe	-	CRESS-15 FeS lost prior to melting	80
15	CRESS-16 Fe	1673	0.0004	15	Fe A	Fe	-	CRESS-16 FeS lost prior to melting	81
16	CRESS-18 Fe	1673	0.0004	120	Fe A	Fe	-	CRESS-18 FeS lost prior to melting	82
17	CRESS-19 Fe	1723	0.0003	15	Fe A	Fe	-	CRESS-19 FeS lost prior to melting	83
10	CRESS-23 Fe	1573	0.0004	15	Fe A	Fe	-	CRESS-23 FeS lost prior to melting	00
18	CRESS-24 FeS	1573	0.0004	15	FeS A	FeS, Fe-Ru-W-Re-Ir alloy	-0.07(9)	-	84
19	CRESS-25 Fe	1623	0.0004	15	Fe A	Fe	-	CRESS-25 FeS lost prior to melting	85
20	CRESS-26 Fe	1773	1	5	Fe A	Fe	-	Performed together with CRESS-26 FeS	86
21	CRESS-26 FeS	1773	1	5	FeS A	FeS, Fe-W-Re-Ir alloy	-0.02(3)	Performed together with CRESS-26 Fe	87
22	CRESS-27 Fe	1773	1	30	Fe A	Fe	-	Performed together with CRESS-27 FeS	88
22	CRESS-27 FeS	1773	1	30	FeS A	FeS, Fe-W-Re-Ir alloy	-0.03(3)	Performed together with CRESS-27 Fe	00
23	CRESS-32 Fe	1773	1	120	Fe A	Fe	-	Performed together with CRESS-32 FeS	69
24	CRESS-32 FeS	1773	1	120	FeS A	FeS, Fe-Ru-W-Re alloy	-0.04(3)	Performed together with CRESS-32 Fe	90
25	CRESS-33-FeS	1573	1	15	FeS A	FeS, Fe-W-Re-Ir alloy	0.00(3)	-	91
26	CRESS-34 FeS	1623	0.0013	15	FeS A	FeS, Fe-Ru-W-Re-Ir alloy	-0.06(5)	-	92
27	CRESS-35 FeS	1673	0.0010	15	FeS A	FeS, Fe-Ru-W-Re-Ir alloy	-0.09(2)	-	93
	CRESS-36 FeS	1723	0.0010	15	FeS A	FeS, S-poor Fe-rich alloy	-0.11(2)	-	00
28	CRESS-37 FeS	1773	0.0010	5	FeS A,	FeS, S-poor Fe-rich alloy	-0.13(6)	CRESS-37 Fe lost prior to melting	94
29	CRESS-38 Fe	1773	0.0010	30	Fe A	Fe	-	CRESS-38 FeS lost prior to melting	95
30	CRESS-39 FeS	1773	0.0010	15	FeS A	FeS, S-poor Fe-rich alloy	-0.15(4)	- CRECC 40 F-C hast animate multime	96
31	CRESS-40 Fe	1772	0.0009	120	Fe A	Fe	-	CRESS-40 FeS lost prior to melting	97
32	CRESS-42 Fe	1772	0.0010	60	Fe A	Fe	-	CRESS-42 FeS lost prior to melting	98
22	CRESS-44 Fe	1773	0.0010	с СО	Fe A	re Canon Fourish allow	-	- Cirrifornt Class	00
33	CKESS-40 FCS	1//3	0.0010	15	FeS A	S-poor re-rich alloy	-1.99(22)	Significant S 1088	99
34	ESS-1-150-CK1 FES	1373	1	15	Fe A	Fes, re-vv-Re-II alloy	-0.02(10)	-	100
35	ESS-1-150A1 FC	1772	1	10	Fe A	Fe	-	-	101
36	ESS-1-15001 FeS	1773	1	30	FeS A	Fes Fe-W-Re-Ir allow	- $-$ 0.02(7)	-	102
37	ESS-V-140-CR1 FeS	1673	0 0003	15	FeS A	FeS S-poor Fe-rich \pm Fe-W-Re-Ir allow	-0.02(7)		103
38	ESS-V-140-CR1 FeS	1673	0.0003	315	FeS A	FeS S-poor Fe-rich allov	-0.47(15)		104
00	ESS-V-140-CR2 FeS	1673	0.0003	60	FeS A	FeS S-poor Fe-rich \pm Fe-W-Re-Ir allov	-0.44(10)		104
39	ESS-V-140-CR4 FeS	1673	0.0003	120	FeS A	FeS S-poor Fe-rich allov	-100(138)	_	105
40	NFSS-1-135CR1-Fe	1623	1	15	Fe B	Fe	-	_	106
41	NESS-1-135CR1-FeS	1623	1	15	FeS B	FeS Fe-W-Re allov	0.02(5)	_	107
42	NESS-1-145CR1-Fe	1723	. 1	15	Fe B	Fe	-	-	108
43	NESS-1-145CR1-FeS	1723	1	15	FeS B	FeS	-0.01(4)	-	109
44	NESS-1-150CR1 Fe	1773	1	5	Fe B	Fe	_	-	100
44	NESS-1-150CR2 Fe	1773	1	15	Fe B	Fe	-	_	110
45	NESS-1-150CR3 Fe	1773	1	90	Fe B	Fe	-	_	111
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^a FeS A = FeS + 0.1 mole % of Cr, Co, Ni, Cu, Ge, Mo, Ru, Pd, Ag, W, Re and Ir; Fe A = Fe + 0.1 mole % Cr, Co, Ni, Cu, Ge, Mo, Ru, Pd, Ag, W, Re, Ir; FeS B = FeS + 0.1 mole % of Ni, Cu, Ge, Mo, Ag, W, Re; Fe B = Fe + 0.1 mole% of Ni, Cu, Ge, Ag. b FeS = quenched FeS liquid; Fe = quenched Fe liquid; S-poor Fe-rich alloy = immiscible S-poor quenched Fe liquid. Note: PGE-rich alloys were generally very small (<10 um). c Early loss of experiments prior to melting occurred due to escape of the sample during initial depressurization.

3.3. Effect of high-temperature degassing on elemental abundances 52

Ni – normalized evaporative loss factor of element i $f^{(i/Ni)} = \frac{f^i}{f^{Ni}}$

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The potential evaporative loss of element i was quantified by considering the ratio between the concentration of element i in the reference material and the experimental sample, respectively:

Evaporative loss factor of element $i(f^i)$

$$\stackrel{60}{\stackrel{61}{}_{62}} = \frac{\text{concentration of element } i \text{ in experimental sample (ppm)}}{\text{concentration of element } i \text{ in reference material (ppm)}}$$

$$\stackrel{63}{}_{64} \qquad (1)$$

65 The evaporative loss factors from Eq. (1) were then normalized to 66 Ni:

The main reason for using Ni as a reference is that it is highly homogeneously distributed throughout the experiments, for both Fe and FeS liquids (Fig. 2). Nickel is also a major element in magmatic iron meteorites (Scott and Wasson, 1975). However, the above approach assumes that Ni behaves non-volatile at the experimental conditions of interest. This can be tested by comparing the behavior of a nominally highly refractory element such as Ir with Ni. Consideration of the Ir/Ni ratio shows no systematic variation, i.e., no increase of the Ir/Ni ratio with run time, pressure or temper-130 ature, suggesting Ni is not volatile under the experimental condi-131 tions explored here (see also sections 3.3.2 and 3.3.3.). Absolute 132

(2)

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Fig. 2. Variability of measured volatile concentrations along horizontal and vertical LA-ICP-MS and/or grid spot transects on experimental run products CRESS 23 (Fe), CRESS 24 (FeS) and CRESS 7 (FeS, Fe). No significant systematic variability in elemental concentrations is observed throughout the samples. The relatively large variability in W and Re concentrations in FeS liquid is due to their low solubility in FeS liquid, resulting in the formation of (Ru)-W-Re-Ir rich phases (see text for detailed discussion). Uncertainties on individual spots are smaller than symbol sizes in all cases.

concentrations of Ni are also similar or deviate positively from the measured Ni content of the high P-T synthesized starting mate-rials (up to +1800 ppm for FeS liquids and +700-800 ppm for Fe melts, Fig. S.5), confirming that Ni was not lost but rather en-riched through preferential evaporation of Fe and/or S. Evaporative loss factors were predominantly based on LA-ICP-MS derived mea-surements, except for S and for experiments containing Ru-, W-, Re- and/or Ir-bearing HSE nuggets that were too small to be mea-sured by LA-ICP-MS. For S and the latter experiments evaporative loss factors were based on EPMA measurements. Figs. 3, 4 and S.6 to S.18 show the logarithmic evaporative loss factors for all of the elements of interest (Table S.4; Appendix section A.2).

3.3.2. FeS liquid experiments

Analyses of the FeS liquids degassed at 1 bar show no evidence of volatile loss up to 1823 K for S, Fe, Cr, Co, Ni, Cu, and Pd (Fig. 3, Table S.4; Fig. S.6 to S.11). However, Ge, Mo and Ag and most likely Ru, Re, W and Ir are affected by volatility-related loss at these conditions (Fig. 3, Table S.4). Results for FeS melts degassed un-der vacuum at \sim 0.001 bar imply, that the elements S, Cu, Ge, Mo, Ag are all evaporated at 1773 K (Fig. 3, 4), as well as Ru, Re, W and Ir (Table S.4, Fig. S.6 to S.12). The decrease of elemental volatility with increasing total pressure is discussed at length in previous studies (e.g., Richter et al., 2011; Sossi et al., 2020). It is a result of a shorter mean free patch (i.e., slower diffusion) of the evaporating species at ambient pressure, relative to vacuum, therefore yielding lower evaporation rates at ambient pressure. Elements Ru, Re, W and Ir are virtually in all experimental samples depleted by up to several orders of magnitude. However, the P-T-time depen-dencies are difficult to derive within the present study due to their low solubility in FeS matte and the resulting heterogeneous distribution.

3.3.3. Fe liquid experiments

Post-experimental analyses of the Fe liquids degassed at room pressure show that only Ag was lost considerably (up to 99.99%) within the studied temperature range (1673–1823 K) (Table S.4, Fig. 4; Fig. S.13 to S.18). Under the investigated redox conditions (~CCO buffer), post-experimentally measured abundances of Cr, Co, Ni, Cu, Ge, Mo, Ru, Pd, W, Re and Ir suggest no loss of these elements at temperatures of up to 1823 K at 1 bar (Fig. 4, Table S.4, Fig. S.13 to S.18). Decreasing the pressure from 1 bar to ~0.001 bar increases the volatility of Cu, Ge, Ag at 1673–1773 K resulting in $f^{(i/Ni)}$ values that are up to 5 orders of magnitude lower relative to the starting compositions. However, the other elements considered do not evaporate at these conditions (Fig. 3, Table S.4, Appendix section A.2).

3.3.4. The effect of S and C on elemental volatility in metallic melts

Comparing the results for Fe and FeS liquid shows that the presence of S greatly affects the volatility of Cu, Ge, Mo, Ru, Ag, W, Re and Ir (Table S.4, Fig. 3). In case of Ge, Mo, Ru, W, Re and Ir, the volatility is significantly increased by the addition of S at a given set of P-T-time conditions, whereas for Ag and Cu it is strongly decreased. It should be noted that the importance of S on Ge volatility was already suggested from previous thermodynamic calculations and volatility experiments relevant to silicate melts and fumarolic systems (Sears, 1978; Wai and Wasson, 1979; Renggli and Klemme, 2020). Generally, nominally sulfide-loving (chalcophile) elements such as Ag and Cu are observed to be less volatile in FeS liquid, compared to Fe liquid. This can be explained

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Fig. 3. Evaporative loss factors, normalized to Ni (Eq. (1), (2)), versus time for FeS and Fe liquids. Yellow stars and solid lines indicate the initial ratio prior to degassing.
 Reported uncertainties are based on maximum errors on LA-ICP-MS measured abundances in the high-pressure melted starting mixture and on experimental run products.
 Also shown (where available) are the modeled dependencies from Table 2. The data labels indicate whether the experiment was conducted simultaneously with a Fe or FeS run or if it was performed without another experiment present. The label #2 indicates the use of the second starting composition NESS FeS or Fe.

by the high activity coefficients of these elements in Fe liquid (e.g., Swartzendruber, 1984; Wood et al., 2014; Norris, 2017 and refer-ences therein), increasing their evaporative potential. On the other hand, nominally iron-loving (siderophile) elements such as Ge and Mo have high activity coefficients in FeS liquid (Wood et al., 2014; Norris, 2017 and references therein), promoting their evaporation from FeS liquid relative to Fe liquid. The strong effect of S on el-ement volatilities is also evident from the experimental samples that experienced minor S cross-contamination or significant S loss (see discussion in section 3.2 and Fig. S.4). For example, Ge be-haves significantly more volatile in run CRESS-32 Fe, that suffered from 0.75 wt.% S cross-contamination, compared to the expected trend of uncontaminated S-free Fe liquid evaporation experiments (Table S.4, Fig. S.14). On the other hand, chalcophile element Ag be-haves less volatile in the presence of S, again consistent with the higher-than-expected Ag evaporative loss factor derived for experi-ment CRESS-32 Fe (Table S.4, Fig. S.16). Elements Mo, W and Re are volatile in S-contaminated run CRESS-38 Fe, whereas in nominally S-free experiments they are not (Table S.4). Sample CRESS-46 suffered significantly more S loss relative to experiments performed at comparable *P-T*-time conditions, resulting in more volatile behavior of Cu and less volatile behavior of Mo, Ru, W, Re and Ir (Fig. 3, Table S.4). The presence of S is therefore a key parameter in establishing the volatilities of Cu, Ge, Ag, Mo, Ru, W, Re and Ir.

Carbon, inevitably present due to the use of graphite buckets and/or a CO furnace atmosphere, may also affect the volatility of the elements of interest. However, all experiments were conducted in graphite buckets and the effects of C can therefore not be iso-lated at this point. However, given the observed systematics of elemental volatility for Fe and FeS melts that qualitatively reflect their activity coefficients in Fe and FeS melt, it is likely that the volatility of carbon-loving elements is decreased in C-saturated Fe liquid and vice-versa. Elements W and Mo are both carbon-loving (Siebert et al., 2011) and are expected to be more volatile in C-

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5896697e^{-0.00808116 * T(K)}

65090e^{-0.00531401 * T(K)}

Table 2

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Cu/Ni (Fe) – vacuum

Ge/Ni (Fe) - vacuum

Ag/Ni (FeS) - vacuum

Ag/Ni (Fe) - vacuum

2 Summary of the parameterizations describing elemental volatility for FeS and Fe liquids and the fit parameters for temperature, time (t). The fits were obtained for (1) all data or (2) all data excluding plateau values which do not vary with experimental run time. The last column lists the lag time (t₀) correction parameters, where applicable. 3 4 R^2 B (1/T (K)) C (log N Lag time (t₀) in min Log А (experimental run 5 time in min)) 6 All data 7 7701e^{-0.00402053 * T(K)} -1.286(1093)0.83 S/Ni (FeS) – vacuum 3310(1874) -0.725(116)11 8 1496(4820) 0.69 Cu/Ni (FeS) - vacuum n.s.s.^a -1498(354)10 10 q 5032367e^{-0.00801547 * T(K)} Cu/Ni (Fe) - vacuum -9.912(1507)19855(2397) -2.245(164)14 0.97 10 Ge/Ni (FeS) - vacuum Highly volatile _ 11 Ge/Ni (FeS) - 1 bar Highly volatile^b 12 447837e^{-0.00647200 * T(K)} Ge/Ni (Fe) - vacuum -9.574(2833)20335(4507) -2.768(308)15 0.92 13 133086e^{-0.00600614 * T(K)} Mo/Ni (FeS) - vacuum -2.284(1054)4676(1817) -0.686(103)9 0.87 14 Ru/Ni (FeS) – vacuum Volatile Ru/Ni (FeS) - 1 bar 15 Volatile _ 11 16 Ag/Ni (FeS) - vacuum -2.293(1407)n.s.s.^a -1.407(320)0.68 11523(6034) -0.907(399) Ag/Ni (Fe) - vacuum -9.538(3774)13 0.56 17 Ag/Ni (Fe) – 1 bar -6.103(2869)12845(4963) -1.936(206)14 0.90 18 W/Ni (FeS) - vacuum Volatile 19 W/Ni (FeS) – 1 bar Volatileb 20 Re/Ni (FeS) - vacuum Volatile _ 21 Re/Ni (FeS) - 1 bar Volatile _ _ 22 Ir/Ni (FeS) - vacuum Volatile 23 Ir/Ni (FeS) - 1 bar Volatile 24 Excluding plateau values

^a n.s.s. = not statistically significant. ^b due to high volatility samples were (almost) fully degassed at any pressure, temperature and time considered. ^c Assessment remains uncertain due to highly heterogeneous distribution in FeS matte as a result of their low solubility and resulting nugget formation.

-2.275(204)

-3.166(432)

-2.248(703)

-1.484(611)

20881(2255)

19164(4780)

10560(6385)

n.s.s.^a



-10.484(1453)

-8.408(3166)

-1.351(826)

-8304(4056)

Fig. 4. Evaporative loss factors, normalized to Ni (Eq. (1), (2)), versus temperature, for Fe liquids. The time of 15 minutes represents the experimental run time, i.e., not incorporating lag time. See Fig. 3 caption for additional details.

free Fe liquid. Sulfur, Cu, Ge and Ag are carbon-avoiding (Siebert et al., 2011; Norris, 2017 and references therein) and therefore will likely behave relatively less volatile in C-free Fe liquid, relative to C-saturated Fe melt. Finally, it is expected that the effects of C in FeS liquid on elemental volatility are small or negligible, given the very low solubility of C in such melts (i.e., 0.2–0.3 wt.% C; e.g., Zhang et al., 2018).

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3.4. Empirical parameterizations describing volatilities

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Application of commonly used thermodynamic models to our data (e.g., Sossi et al., 2019) would require insights into the species that are evaporated, which in many cases are currently not or poorly constrained and/or could also involve multiple species depending on *P-T* conditions. We therefore obtained empirical parameterizations describing the volatilities of the elements of interest (S, Cu, Ge, Ag, Mo) as a function of experimental run time (t, in min) and temperature (*T*). The experimental data (Table S.4) were fitted to Eq. (3) using multiple linear regressions:

$$\log f^{(i/Ni)} = A + B\left(\frac{1}{T(K)}\right) + C\left(\log(\text{experimental run time}_{(\min)})\right)$$
(3)

where T is temperature in K and t is time in minutes. Equation 124 (3) was chosen to provide a reasonable predictor of the experi-125 mental data as a function of time and temperature. The experi-126 127 mental run time is different than the effective degassing time as a lag time may exist between heating and melting of the sam-128 ples (e.g., Sossi et al., 2019). Pressure was also not included as a 129 term in Eq. (3), as only two pressure anchor points are available to 130 constrain the effects of pressure. Multiple linear regressions were 131 performed separately for data obtained for FeS or Fe melts and for 132



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Fig. 5. Modeled Ni-normalized evaporative loss factors of the elements of interest (where available), calculated using Eq. (3) in conjunction with the fit parameters from Table 2, at 10⁻⁴ bar for FeS and/or Fe liquids, as a function of evaporation time. Green lines indicate modeled dependencies for which no temperature effects could be derived (see main text).

data obtained at vacuum or at 1 bar. Multiple linear regressions were performed using RegressIt[©], an openly available Excel add-in package. Fit parameters were considered to be statistically significant if the Pearson correlation coefficient (p) is <0.10.

Table 2 provides a summary of the potential volatile behavior of the elements of interest and the derived fit parameters (where applicable) and Fig. 5 shows some of these results graphically. The lack of statistically significant parameters in Table 2 for some of the elements generally indicates that the volatility of the element of interest is little affected by the parameters considered. For Cu, Ge and Ag in FeS liquid, no temperature dependencies on their volatility could be constrained, independent of pressure. This is

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Table 3

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Derived reaction rate constants (k₁ values) for the elements of interest for each set of temperature and pressure conditions. The y-axis intercept was forced to 0 with slope

	Composition	T (K)	Pressure	Time range (min)	k i (cm/min)	Slope	1SE	R ²	N	Comment
S	FeS	1773	1 bar	5-120	6.00 x 10 ⁻⁵	-1.20 x 10 ⁻³	3.00×10^{-4}	0.78	6	All data
S	FeS	1673	vacuum	15-120	9.80 x 10 ⁻⁴	-1.95 x 10 ⁻²	1.80 x 10 ⁻³	0.97	5	All data
S	FeS	1773	vacuum	5 - 60	3.66 x 10 ⁻³	-7.31 x 10 ⁻²	8.90 x 10 ⁻³	0.97	3	All data
Cu	FeS	1673	vacuum	15-120	1.50 x 10 ⁻³	$-3.00 \text{ x } 10^{-2}$	8.10 x 10 ⁻³	0.77	5	All data
Cu	FeS	1773	vacuum	5-60	3.93 x 10 ⁻³	-7.85 x 10 ⁻²	2.15 x 10 ⁻²	0.87	3	All data
Cu	Fe	1673	vacuum	15-120	2.86 x 10 ⁻³	-5.72 x 10 ⁻²	3.80 x 10 ⁻³	0.99	3	All data
Cu	Fe	1773	vacuum	5-120	3.39 x 10 ⁻³	-6.77 x 10 ⁻²	1.57 x 10 ⁻²	0.82	5	All data
Cu	Fe	1773	vacuum	5-60	5.70 x 10 ⁻³	$-1.14 \text{ x } 10^{-1}$	1.94 x 10 ⁻²	0.92	4	Excluded plateau value CRESS-40-Fe
Ge	FeS	1773	1 bar	-	-	-	-	-	-	Fitting not possible due to highly volatile behavior
Ge	FeS	1673	vacuum	-	-	-	-	-	-	Fitting not possible due to highly volatile behavior
Ge	FeS	1773	vacuum	-	-	-	-	-	-	Fitting not possible due to highly volatile behavior
Ge	Fe	1773	1 bar	5-90	1.35 x 10 ⁻⁴	-2.70 x 10 ⁻³	1.10 x 10 ⁻³	0.42	10	All data
Ge	Fe	1673	vacuum	15-120	2.80 x 10 ⁻³	-5.60×10^{-2}	4.30 x 10 ⁻³	0.99	3	All data
Ge	Fe	1773	vacuum	5-120	4.08 x 10 ⁻³	-8.16 x 10 ⁻²	1.73 x 10 ⁻²	0.85	5	All data
Ge	Fe	1773	vacuum	5-60	6.82 x 10 ⁻³	-1.36 x 10 ⁻¹	1.67 x 10 ⁻²	0.96	4	Excluded plateau value CRESS-40-Fe
Мо	FeS	1673	vacuum	15-120	7.05 x 10 ⁻⁴	-1.41 x 10 ⁻²	2.70 x 10 ⁻³	0.87	5	All data
Мо	FeS	1773	vacuum	-	-	-	-	-	-	Fitting not possible due to lack of da excluded CRESS-46
Ag	FeS	1673	vacuum	-	-	-	-	-	-	Fitting not possible due to highly volatile behavior
Ag	FeS	1773	vacuum	-	-	-	-	-	-	Fitting not possible due to highly volatile behavior
Ag	Fe	1773	1 bar	5-90	4.62 x 10 ⁻³	-9.23 x 10 ⁻²	1.08 x 10 ⁻²	0.90	10	All data
Ag	Fe	1673	vacuum	15-120	2.86 x 10 ⁻³	-5.72 x 10 ⁻²	6.74 x 10 ⁻²	0.50	3	All data
Ag	Fe	1773	vacuum	5-120	5.99 x 10 ⁻³	-1.20×10^{-1}	4.42 x 10 ⁻²	0.64	5	All data
Ag	Fe	1773	vacuum	5 - 60	1.12 x 10 ⁻²	-2.23×10^{-1}	7.59 x 10 ⁻²	0.74	4	Excluded plateau value CRESS-40-Fe

because they behave either too volatile (Ge, Ag) or insufficiently volatile (Cu) at these conditions (Fig. 3, 4). As previously discussed, 33 no reliable fits could be obtained for Ru, W, Re and Ir, predominantly due to their heterogeneous distributions in the sulfide melts as nuggets, resulting in very large uncertainties of their derived bulk abundances (Fig. S.10, S.11, S.12 and Table S.2). We recommend that their potentially volatile behavior should be accurately constrained at very low initial concentrations (i.e., ppm levels) in a future study.

However, some parameterizations yield modeled log $f^{(i/Ni)}$ val-41 ues that exceed 0 at short timescales. This is considered to reflect 42 the "lag time" previously observed by Sossi et al. (2019), that de-43 pends on experimental arrangement, such as heating time and 44 45 thermal conductivity of the starting material, the use of a powder 46 instead of a solid starting material, the grain size and the over-47 all size of the sample. We therefore added an element-specific 48 lag-time parameter to each parameterization to account for this, 49 which in turn also depends on temperature (i.e., higher temper-50 ature yields a shorter heating time required for melting of the 51 sample): 52

Effective degassing time (t_d in min)

(4)= experimental run time (t in min) – lag time (t₀ in min)

56 The actual experimental run time minus the lag time is defined as 57 the "effective degassing time" or t_d (Eq. (4)). The lag time is deter-58 mined for each element using the difference between the modeled 59 log(i/Ni) value and 0 at the experimental run time of 0 at a given 60 temperature. These results show that the lag time as a function 61 of temperature is most accurately described using exponential fits 62 (Fig. S.19) and that these vary between 0-17 min at 1573 and 2-5 63 min at 1823 K, depending on the element. We emphasize that 64 the latter lag times are strictly only valid within the experimen-65 tal temperature range, i.e., between 1573-1823 K, and cannot be 66 extrapolated to lower temperatures.

We also calculated the reaction rate constant (k_i) of the evaporation of the elements of interest using a fully thermodynamic approach, while considering the radius (r) of the sample (0.15 cm), the time (t in min) and the natural logarithm of the ratio between the initial concentration (C_0) and the final concentration (C)(Tsuchiyama et al., 1981; Sossi et al., 2019, see Supplementary Information File section A.3; Table 3):

$$\ln(C/C_0) = -\frac{3k_i t}{r} \tag{5}$$

The slope was derived by consideration of $\ln(C/C_0)$ of each element versus time in minutes at a given pressure and temperature. The k_i values were then calculated by Eq. (6)

$$k_i = \frac{\text{slope} * r}{-3} \tag{6}$$

Table 3 lists the derived k_i values. As expected, k_i values increase with temperature and also vary significantly for FeS and Fe melt, as observed earlier in this study (Fig. S.20).

The plateau values observed for Cu. Ge and Ag for FeS and/or 117 Fe liquid are potentially the result of the analytical difficulties of 118 measuring their elemental abundances which are close to detec-119 tion limits. However, it could also reflect a steady state between 120 the furnace atmosphere and sample or (an)other process(es). The 121 incorporation of these measurements in the parameterizations may 122 123 result in erroneous results and therefore the data of Cu and Ge for 124 Fe at vacuum and Ag for both Fe and FeS liquid at vacuum were 125 also parameterized by excluding the aforementioned plateau values (Table 2). However, the results are near-identical, except for 126 127 a slightly faster loss at a given temperature, pressure and compo-128 sition. Finally, Table 2 shows that the fit for Ag in the Fe system 129 at 1 bar, based on values that far exceed the detection limit, is near-identical to the fit for Ag in the same system at high vacuum. 130 Therefore, we conclude that the parameterizations and correspond-131 ing lag times that were obtained in the earlier section are robust 132

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throughout the experimental range and are not significantly affected by the incorporation of plateau values.

4. Discussion

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4.1. Comparison with currently applied volatility models

8 The 50% condensation temperatures (Lodders, 2003; Wood et q al., 2019) are often used as a proxy for elemental volatility for a 10 wide range of planetary processes (e.g., Wai and Wasson, 1979; 11 Campbell and Humayun, 2005). However, the nebular gas under 12 which condensation occurred was highly reducing ($\Delta IW = -7$; 13 Wood et al., 2019), which is likely not relevant to evaporation from 14 the large majority of metal-rich molten planetesimals. Soon after 15 dissipation of the primordial H-rich atmosphere, silicate/metal-gas 16 equilibria would instead be governed by the Fe-FeO equilibrium, 17 yielding much more oxidized conditions (i.e., $\Delta IW - 1$ to -2.5; 18 Righter et al., 1998; Wood et al., 2006). This large difference in re-19 dox state could significantly affect the predicted volatility of the 20 elements of interest. Indeed, the relevant volatility sequence pre-21 dicted by the condensation temperature models would be S, Ag 22 < Ge < Cu < Mo, Ru < Re, W, over a range of \sim 700 to 1740 23 K at 0.0001 bar (Wood et al., 2019). At these pressures, our ex-24 perimental results for Fe liquid suggests a similar sequence, i.e., 25 Ag < Ge < Cu, while Cr, Co, Mo, Pd Ru, Re, W were found to be 26 not volatile. However, this is significantly different for FeS liquid, 27 where volatility increases in the order of Ge, Ag < Cu < S, Mo, Ru, 28 W, Re, Ir < Cr, Co, Pd. The presence of S thus significantly affects 29 their volatility which agrees with previous experimental and ther-30 modynamic studies that found major effects of silicate melt and 31 gas-phase composition on evaporation behavior (e.g., Renggli and 32 Klemme, 2020; Pangritz et al., 2022). The comparison also clearly 33 shows that 50% condensation temperatures are not directly appli-34 cable to evaporation processes on metal-rich planetesimals. 35

4.2. Evaporative loss from the IVB parent body? 37

38 We now demonstrate the applicability of our experimental data 39 and the new parameterizations to assess potential evaporative loss 40 from the IVB parent body, which is the source of the IVB iron me-41 teorites, the most volatile element-depleted magmatic iron mete-42 orite suite. The volatile element contents of the IVB iron meteorites 43 cannot be directly used as bulk parent body concentrations, as 44 the suite has experienced extensive magmatic differentiation (up 45 to 86% of metal crystallization), as evidenced from major, minor 46 and trace element systematics (e.g., Campbell and Humayun, 2005; 47 Zhang et al., 2022). We therefore used reconstructed IVB parent 48 melt compositions (Chabot, 2004 for S; Campbell and Humayun, 49 2005 for all other elements) in conjunction with a CI chondritic 50 bulk composition (taken from Alexander, 2019) to obtain volatile 51 element depletion factors of the elements of interest (Table S.1). It 52 should be noted that no uncertainties are reported for these es-53 timates in the latter studies. No estimates for Ag for IVB parent 54 melt compositions are currently available. We therefore assumed 55 the average of two reported parent body melt concentrations for 56 Muonionalusta (1 and 3 ppb, respectively), a group IVA iron mete-57 orite, from Horan et al. (2012) (Table 2). Finally, Mo isotopes have 58 also been used to infer a carbonaceous chondritic heritage of the 59 IVB parent body (Budde et al., 2016), justifying our choice of the 60 IVB parent body bulk composition.

We assumed a 10% uncertainty on previously published parental melt and bulk CI concentrations as no uncertainties were reported in the latter studies. Finally, the assumed metallic parental melt composition does not include the silicate portion of the IVB parent body (Campbell and Humayun, 2005). However, taking the reasonable assumption that equilibrium was (largely) achieved between



Fig. 6. Comparison between modeled Ni-normalized evaporative loss factors of the elements of interest, calculated using Eq. (3) in conjunction with the fit parameters from Table 2 for FeS and/or Fe liquids while incorporating the plateau values, and evaporative loss factors required for explaining reconstructed IVB bulk parent body depletions. Note that Chabot (2004) and Campbell and Humayun (2005) do not report uncertainties on these estimates. Modeling results were obtained at 1673 or 1773 K, evaporation time of 60 and 600 min, all at 10^{-4} bar. The evaporative loss factors for Ru, W, Re Ir were estimated from experimental results obtained at the modeled time and temperature. The red arrow indicates that Ge is potentially more depleted in the experimental samples as Ge contents are often close to the detection limit of 0.1 to 0.2 ppm (Supplementary Table S.1).

the metallic and silicate fractions, all of the elements considered in our model should have partitioned almost completely into the metallic phase (S, Cu, Ge, Mo, Ag), given their moderately to highly siderophile behavior at the estimated redox state of IVB parent body differentiation (Δ IW = -1; Campbell and Humayun, 2005; Steenstra et al., 2017).

The required evaporative loss factors to explain the depletions 114 in the IVB magmatic iron meteorites solely by evaporation were 115 then calculated using Eq. (2) and the previously discussed bulk 116 estimates, and are listed in Table S.4. To assess the likelihood of 117 evaporative loss from a metallic liquid being a major contributor 118 to volatile loss in the IVB parent body, we compared the mod-119 eled evaporative loss factors for FeS and Fe at 10^{-4} bar with the 120 required evaporative loss factors for the IVB parent body. This 121 hypothesis assumes that the IVB parent body core was exposed 122 to space for some time. An important first observation is that 123 volatility trends for nominally volatile elements (S, Cu, Ge, Ag) are 124 reasonably reproduced by all of the modeled scenarios (Fig. 6). 125 However, it is also clear that evaporation of a S-rich melt would 126 certainly result in a significant depletion of Mo, Ru, W, Re and 127 Ir, which is not observed for the IVB parent body, where these 128 elements are actually enriched instead of depleted relative to CI 129 chondrite (Fig. 6). This is a robust conclusion for Mo and to a lesser 130 extent Ru, W, Re and Ir, despite major uncertainties in the exact 131 magnitude of their depletion in experimental samples. Based on 132

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these results alone, it can therefore be concluded that evaporation 2 on the IVB parent body could only have occurred under relatively 3 S-poor conditions. Results for the Fe melt, however, demonstrate 4 how feasible evaporation processes are in explaining the depletions 5 of the elements of interest in the IVB parent body (Fig. 6). Our 6 results are therefore consistent with evaporation of an exposed, 7 molten IVB parent body core, as a result of (a) large impact(s). 8 As proposed by Matthes et al. (2018), for the IVA parent body, q evaporation of Ag is generally an attractive model for explaining 10 the Pd-Ag isotope systematics of these samples as it strongly de-11 pletes Ag and provides a late Pd/Ag fractionation, after which the 12 cores would have rapidly cooled. However, as noted by Matthes 13 et al. (2018), there are some geochemical observations that may 14 not be consistent with (solely) evaporative loss from the IVB parent body core. The reconstructed pre-exposure $\delta^{65}\mathrm{Cu}$ data for the 15 16 IVB suite are slightly negative (Chen et al., 2016), which is the op-17 posite of what would be expected if Cu was predominantly lost 18 through evaporation (Bishop et al., 2012; Chen et al., 2016). Alter-19 natively, Cu could have been extensively evaporated, followed by 20 partial recondensation of Cu in the kinetic regime, yielding a fi-21 nal light δ^{65} Cu value for the IVB parent body. This mechanism has 22 been proposed for reconciling the light δ^{41} K isotopic composition 23 of angrites with the extreme elemental depletion of K in angrites 24 (Hu et al., 2022).

25 It should also be noted that it is unlikely that the IVB par-26 ent body experienced graphite saturation given extensive C loss 27 (e.g., Hirschmann et al., 2021 and references therein) and the de-28 rived evaporative loss factors for Fe-rich melt are likely affected by 29 carbon saturation in our experiments. The possibility can also not 30 be excluded that evaporation of the elements of interest occurred 31 from the silicate melt covering the core, where the present-day 32 IVB meteorite volatile element depletion signature would simply 33 reflect the partitioning of these highly depleted elements from 34 the silicate mantle to the core. Alternatively, incomplete nebular 35 condensation may account for the depletions of (some) of the ele-36 ments of interest. Future work should thus include the evaporation 37 systematics of more volatile and highly volatile elements, with 38 which the potential importance of evaporative loss can be studied 39 in greater detail using multi-element solutions. Finally, the effects 40 of C on evaporative loss from metallic melts needs to be experi-41 mentally tested and constrained. 42

5. Conclusions

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45 The volatility of a suite of siderophile elements was experimen-46 tally assessed under vacuum and room pressures for Fe and FeS 47 melts. Elements S, Fe, Cu, Ge, Ag, Mo, W and likely Ru, W, Ir were 48 found to evaporate at 1573-1823 K, the depletion depending on 49 P-T, composition and duration. Composition of the core-forming 50 liquid strongly affects volatility, with the volatility of Ge, Mo, Ru, 51 W, Re and Ir being strongly increased through the presence of S 52 and Cu and Ag were found to behave less volatile in the presence 53 of S. These results demonstrate the importance of melt composi-54 tion for evaporation systematics. Application of the new thermody-55 namic parameterizations to IVB parent body depletions shows that 56 the latter can be easily explained through evaporation of a S-free 57 or S-poor Fe liquid core under a wider range of temperatures and 58 evaporation durations. Our results are therefore consistent with a 59 potentially important role of evaporative loss on establishing the 60 volatile element depletions in the IVB parent body.

62 CRediT authorship contribution statement

E.S. Steenstra: Writing – original draft, Methodology, Investiga tion, Funding acquisition, Formal analysis, Data curation, Conceptu alization. C.J. Renggli: Writing – review & editing, Methodology, In-

vestigation, Funding acquisition, Data curation, Conceptualization. J. Berndt: Writing – review & editing, Funding acquisition, Formal analysis. S. Klemme: Writing – review & editing, Supervision, Resources, Project administration, Funding acquisition.

Declaration of competing interest

The authors declare that they have no known competing financial interests or personal relationships that could have appeared to influence the work reported in this paper.

Data availability

Data will be made available on request.

Acknowledgements

We thank Maik Trogisch and Beate Schmitte for their excellent sample preparation and assistance with EPMA and LA-ICP-MS analyses, respectively. We also would like to thank Paolo Sossi, an anonymous reviewer and the editor for useful comments that greatly improved the manuscript. This study was funded by SFB TRR-170 and a Marie Curie Postdoctoral Fellowship to E.S.S.; C.R. was funded by the Deutsche Forschungsgemeinschaft (DFG, German Research Foundation) – project 442083018. This is TRR-170 publication no. **204**.

Appendix A. Supplementary material

Supplementary material related to this article can be found online at https://doi.org/10.1016/j.epsl.2023.118406.

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Highlights

- First experimental data of volatile element evaporation from metallic melts.
- Sulfur strongly affects elemental evaporation behavior.
- Volatile element depletions of IVB magmatic iron meteorites can be explained by evaporation.